

AD-A058 192

KEARNEY (A T) INC CHICAGO IL CAYWOOD-SCHILLER DIV
DYNAMIC SAM ENDGAME MODEL, VOLUME 2. USER'S MANUAL.(U)
SEP 77 M A DLOOGATCH, R H ROSE, D S KLUK

F/G 16/4.2

N62269-76-C-0386

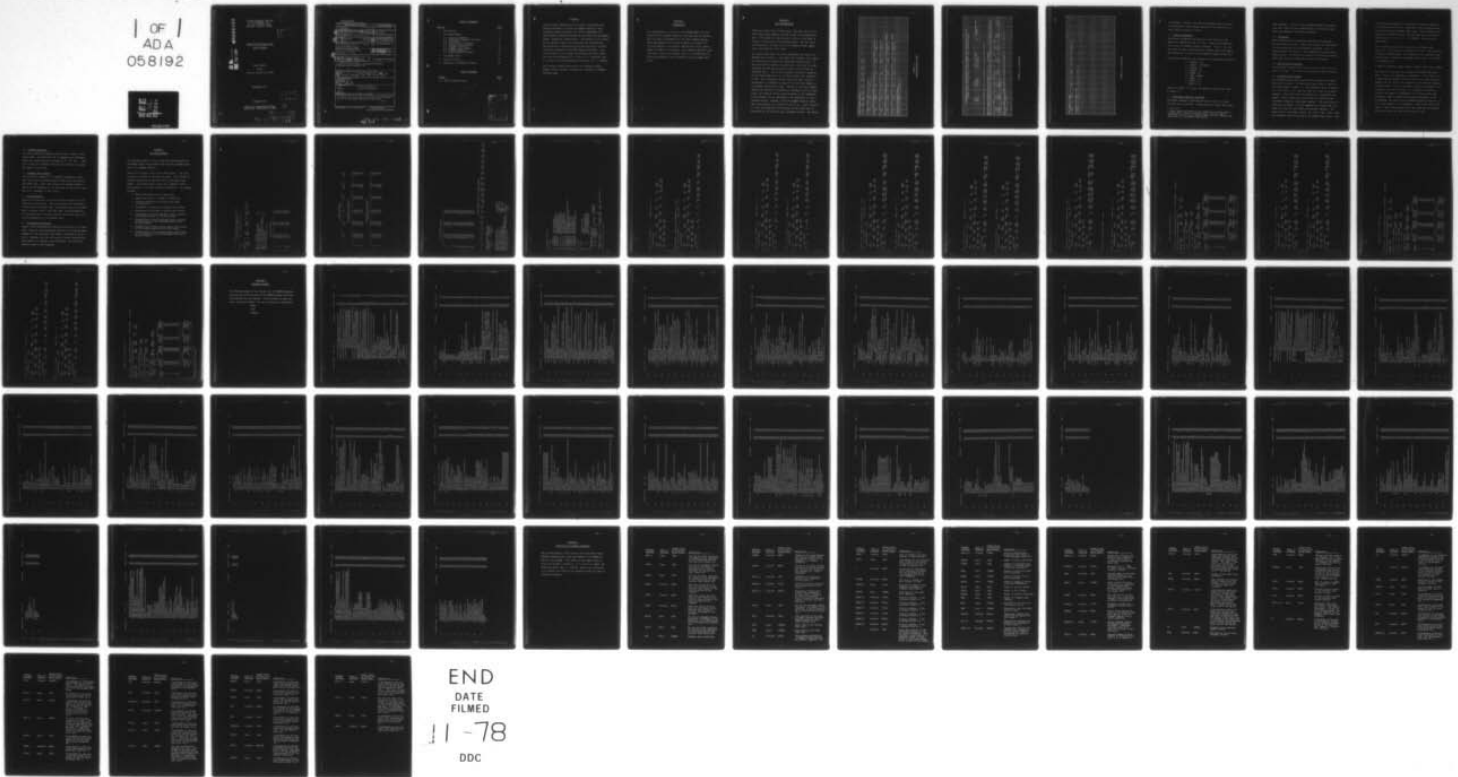
UNCLASSIFIED

CSD-77-200-VOL-2

NL

1 OF 1
ADA
058192

SEP 77



AD No. _____
DDC FILE COPY

ADA058192

CAYWOOD-SCHILLER DIVISION
A. T. KEARNEY, INC.
100 South Wacker Drive
Chicago, Illinois 60606

(2) 46
AO 58050

LEVEL D

DYNAMIC SAM ENDGAME MODEL

USER'S MANUAL

FINAL REPORT

Under

Contract N62269-76-C-0386

SEPTEMBER 1977

Prepared for

NAVAL AIR DEVELOPMENT CENTER
WARMINSTER, PENNSYLVANIA 18974

DDC
RECEIVED
AUG 29 1978
RECEIVED

DISTRIBUTION STATEMENT A

Approved for public release;
Distribution Unlimited

78 08 25 040

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER 77-200-Vol II	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Dynamic SAM Endgame Model, Volume 2, User's Manual. Final Report		5. TYPE OF REPORT & PERIOD COVERED Final Report 7-76 - 9-77
7. AUTHOR(s) M. A. Dloogatch, D. S. Kluk R. H. Rose		6. PERFORMING ORG. REPORT NUMBER
8. CONTRACT OR GRANT NUMBER(s) N62269-76-C-0386		
9. PERFORMING ORGANIZATION NAME AND ADDRESS Caywood-Schiller Div., A. T. Kearney, Inc. 100 South Wacker Drive Chicago, Illinois 60606		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Air Development Center Warminster, PA 18974		12. REPORT DATE September 1977
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) CSD-77-200-VOL-2		13. NUMBER OF PAGES 68
15. SECURITY CLASS. (of this report)		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited. Statement applied September 1977.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report) Final rept. Jul 76-Sep 77,		
18. SUPPLEMENTARY NOTES 72 p.		
19. KEY WORDS (Continue on reverse side if necessary; and identify by block number) SAM Aircraft Survivability Warhead Aircraft Vulnerability Fuze Endgame		
20. ABSTRACT (Continue on reverse side if necessary; and identify by block number) Procedures for using a model for evaluating kill probabilities associated with trajectories and intercept conditions generated by the NADC Dynamic SAM Model are described.		

DD FORM 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

78 08 25 040
406 851

TABLE OF CONTENTS

<u>Section</u>	<u>Page</u>
1. Introduction	1
2. Data Requirements	2
2.1 Control Parameters	6
2.2 Vulnerable Component Locations	6
2.3 Ellipsoids	7
2.4 Glitter Point Locations	7
2.5 Vulnerable Area Tables	7
2.6 Fragment Densities	9
2.7 Fragment Mass Classes	9
2.8 Fuze Parameters	9
2.9 Miscellaneous Constants	9
3. New DSAMAM Output	10
4. Program Listing	25
5. Definition of FORTRAN Variables	56

LIST OF FIGURES

<u>Number</u>	<u>Page</u>
2-1 DSAMAM Endgame Inputs	3

V.1 - A058 050
(77-200 on card)

ADDITION for		
RTIS	White Section	<input checked="" type="checkbox"/>
GOC	Self Section	<input type="checkbox"/>
UNANNOUNCED		<input type="checkbox"/>
JUSTIFICATION		
BY		
DISTRIBUTION/AVAILABILITY CODE		
Dist.	AVAIL. NO. or SPECIAL	
A		

FOREWORD

The activities described in this report in modifying the Dynamic SAM Model to include an endgame capability were performed during the period July 1976 to September 1977 under Contract N62269-76-C-0386 for the Naval Air Development Center, Warminster, Pennsylvania. The purpose of this effort was to develop a means for evaluating kill probabilities associated with trajectories and missile/aircraft intercept conditions generated by the NADC Dynamic SAM Model. This is the second of two volumes constituting the final report. The work was performed by R. H. Rose, M. A. Dloogatch, and D. S. Kluk of the Caywood-Schiller Division of A. T. Kearney.

This volume includes instructions for preparing inputs, sample outputs, program listings and a glossary of FORTRAN variable names.

SECTION 1
INTRODUCTION

As a prerequisite to the use of the DSAMAM model with the addition of an endgame capability the user must be familiar with the input requirements for the basic DSAMAM program. These requirements are covered in detail in Volume II of the Final Report on the Dynamic SAM-Aircraft Study, Report Number C9-2336/120, Autonetics, North American Rockwell Corp. This User's Guide will confine itself to the additional operating requirements which accompany the new endgame capability.

SECTION 2

DATA REQUIREMENTS

There are twelve sets of input cards, each made up of one or more cards, which comprise the new inputs to the DSAMAM program. The format for these inputs is shown on the forms in Figure 2-1 and each set is discussed below. The new inputs are inserted in the data for the old DSAMAM program immediately following the title cards.

All inputs other than the control parameters are read in as FORTRAN real variables. This means that normally they should be entered with an explicitly designated decimal point. If they are entered without a decimal point, they must be right-justified and the implied decimal point will be after the rightmost digit. All of the Cartesian coordinates requested on the input forms are to be in the aircraft body coordinate system. This coordinate system, under the name "stability coordinates," is defined on page 3-22 of the Final Report on the Dynamic SAM-Aircraft Study. Because in the basic DSAMAM program the aircraft is essentially considered to be a single point, the location of the origin relative to the components of the aircraft is not specified in the definition of the coordinate system. However, since the endgame addition represents the aircraft in a variety of ways (e.g., a set of points or a set of ellispoids) the location of the origin must be specified for the aircraft body coordinate system. The choice

DSAMAM ENDGAME INPUTS

[illegible]

VULNERABLE AREA TABLES (6*NCMPS*NWTS*NEVS CARDS) VULNERABLE AREA AS A FUNCTION OF KILL LEVEL, COMPONENT ASPECT, MASS CLASS AND NET STRIKING SPEED. DATA IS NESTED AS FOLLOWS:									
<div> <div> <div>NLEVS KILL LEVELS</div> <div>NCMPS VULNERABLE COMPONENTS</div> <div>6 ASPECTS (BOTTOM, TOP, LEFT, RIGHT, FRONT, REAR, IN THAT ORDER)</div> <div>NWTS FRAGMENT MASS CLASSES</div> </div> </div>									
FOR EACH KILL LEVEL-COMPONENT-ASPECT-MASS CLASS COMBINATION, 1 CARD OF THE FOLLOWING FORMAT									
CONTAINS VULNERABLE AREAS FOR NET STRIKING SPEED=0.0, 0.1, 0.2, ..., 1.0 VNEETH									
VUL(1,1,X)	VUL(1,2,K)	VUL(1,3,K)	VUL(1,4,K)	VUL(1,5,K)	VUL(1,6,K)	VUL(1,7,K)	VUL(1,8,K)	VUL(1,9,K)	VUL(1,10,X)
STATIC FRAGMENT DENSITY (3 CARDS) FRAGMENTS/STERADIAN AT 0°, 10°, 20°, ..., 180° OFF MISSILE NOSE									
STEAR(1)	STEAR(2)	STEAR(3)	STEAR(4)	STEAR(5)	STEAR(6)	STEAR(7)	STEAR(8)	STEAR(9)	STEAR(10)
STEAR(11)	STEAR(12)	STEAR(13)	STEAR(14)	STEAR(15)	STEAR(16)	STEAR(17)	STEAR(18)	STEAR(19)	STEAR(20)
FRACTION BY NUMBER OF ALL FRAGMENTS BELONGING TO EACH MASS CLASS AND AVERAGE WEIGHT IN GRAINS (NWTS CARDS)									
FRACT(1)	FRACT(2)	FRACT(3)	FRACT(4)	FRACT(5)	FRACT(6)	FRACT(7)	FRACT(8)	FRACT(9)	FRACT(10)
FRACT(11)	FRACT(12)	FRACT(13)	FRACT(14)	FRACT(15)	FRACT(16)	FRACT(17)	FRACT(18)	FRACT(19)	FRACT(20)

FIGURE 2-1 (continued)

FUZE CONSTANTS (1 CARD)									
HAFA8C	PMAX	DTMF	PDRF	DICF	PDCF				

MISCELLANEOUS CONSTANTS (1 CARD)									
VREF100	RM155	CDR	V%						

FIGURE 2-1 (continued)

is arbitrary; however, the user will probably wish the point to correspond to some natural feature of the aircraft (e.g., nose, center of gravity, pilot).

2.1 Control Parameters

The control parameters are read in on the first card and define the number of cards to follow. These nine parameters are read in as FORTRAN integer variables. That is, the numbers must be right-justified and no decimal points may appear. The definitions of each of the parameters appear in Section 5.

The control parameters are limited by the following constraints:

$$\begin{aligned}1 &\leq \text{NCOMPS} \leq 25* \\0 &\leq \text{NDUBLY} \leq [\text{NCOMPS}/2] \\0 &\leq \text{NSHLDS} \leq 25 \\0 &\leq \text{NBLAST} \leq 25 \\0 &\leq \text{NDHNC} \leq 25 \\0 &\leq \text{NDHC} \leq \text{NDHNC} \\1 &\leq \text{NGLIT} \leq 25 \\1 &\leq \text{NLEVS} \leq 4* \\1 &\leq \text{NWTS} \leq 10*\end{aligned}$$

where the symbol $[\]$ is read "the greatest integer less than or equal to."

2.2 Vulnerable Component Locations

Vulnerable component locations are read in, one to a card, with the units to be feet. There must be at least one vulner-

* These limits are based on the assumption of being able to utilize 300K (octal) of computer core. If less core is available, one or more of these numbers must be reduced (see discussion of vulnerable area inputs).

able component. If the control parameter NDUBLY is greater than zero, then the first NDUBLY pairs of vulnerable components are assumed to be doubly vulnerable.

2.3 Ellipsoids

There are four sets of ellipsoid centroids and semi-axes. The units are to be feet. Each card contains the coordinates of one centroid and the corresponding semi-axes. Any of these sets may be omitted if the corresponding control parameter is zero. If there are no direct-hit-no-kill-ellipsoids, then there can be no direct-hit-with-kill-ellipsoids.

2.4 Glitter Point Locations

Glitter point locations are read in, one to a card, with the units to be feet. At least one glitter point must be present.

2.5 Vulnerable Area Tables

The vulnerable area tables are the most extensive and complicated set of inputs. The nesting of these cards is shown on the second page of Figure 2-1. The outermost level of nesting is by kill level. All cards for each kill level are grouped together. The second level of nesting is by vulnerable component. Within a particular kill level all cards for each vulnerable component are grouped together. The third level of nesting is by aspect. For any component at a particular kill level the cards for each aspect are grouped together. The aspects are in the order: bottom, top, left, right, front, rear. The innermost level of nesting is by fragment mass class. Thus,

for a particular aspect of a particular vulnerable component at a particular kill level, there must be one vulnerable area input card for each fragment mass class. Each individual card contains 11 vulnerable areas, one for each value of striking speed from 0.0, 0.1, 0.2, ..., $\geq 1.0 \cdot \text{VNETHI}$. The units are square feet.

The vulnerable area data is read into the FORTRAN array $\text{VUL}(I,J,K)$. The subscript I denotes kill level. The subscript J denotes striking speed. The subscript K is a composite combining aspect, component and fragment mass class. The formula for computing K is:

$$K = \text{NWTS} \cdot (6 \cdot \text{component number} + \text{aspect number} - 7) + \text{mass class number}.$$

The array VUL requires core storage of $66 \cdot \text{NCOMPS} \cdot \text{NWTS} \cdot \text{NLEVS}$ words. Thus, to accommodate 25 components, 4 kill levels and 10 mass classes requires 66,000 words for VUL alone and thus demands the full 98,304 word capacity of the CDC 6600 computer system at NADC. Since it requires a special arrangement to be allowed to use this much core, it is normally desirable to restrict the number of components, kill levels and/or mass classes in order to reduce the storage requirements of VUL. For example, the listing of the DSAMAM program in Section 4 is for a case limited to 12 components, 1 mass class, and 2 kill levels. Thus, VUL requires only 1,584 words and the program can be run using less than 40,000 words of core.

2.6 Fragment Densities

The static explosion fragment density data is read in from three cards. The densities are in fragments per steradian. There are values read in for angles of 0° , 10° , 20° , ..., 180° for a total of 19 entries (8 on each of the first two cards and three on the third).

2.7 Fragment Mass Classes

The fraction by number of all fragments belonging to each mass class and the average weight of each class are read in from NWTS cards. Each card contains the average weight in grains of the fragments in one class and the fraction by number of all fragments in that class.

2.8 Fuze Parameters

There is one card used to read in various constants for the radar and contact fuzes. This card contains the half-angle of the cone of the radar fuze, the maximum range of the radar fuze, the delay time of the radar fuze, the dud probability for the radar fuze, the delay time of the contact fuze, and the dud probability of the contact fuze.

2.9 Miscellaneous Constants

Finally, four miscellaneous constants are read in on one data card. These are the normalizing value for the striking speed argument in the vulnerable area tables, the range at which a miss is assumed given that the point of closest approach has been passed, the fragment drag coefficient, and the static emission speed of the fragments.

SECTION 3
NEW DSAMAM OUTPUT

The following pages of this section show those portions of the DSAMAM output which differ from the basic DSAMAM output due to the endgame addition.

There are two types of new output which appear. The first is simply a listing of the new input data. This listing is complete except for the omission of the vulnerable area tables. The second output type is the "summary of kill" which appears at the time of missile detonation. The summary includes:

1. Time of detonation due to radar fuze.
2. Range from missile to target at detonation.
3. Inertial coordinates of missile and target at detonation.
4. Coordinates of missile in aircraft body system.
5. Coordinates of aircraft in missile body system.
6. Probabilities of each component having survived this single missile at all kill levels.
7. Probabilities of each component having survived all missiles up to and including this one at all kill levels.
8. Probabilities of the aircraft having been killed by this single missile at all kill levels.
9. Probabilities of the aircraft having been killed by all missiles up to and including this one at all kill levels.

TEST CASE
DEMONSTRATE AIR CRAFT TRAJECTORY GENERATION
AND NEW MISSILE GUIDANCE MODE

ST FLIGHT THIS IS REGULAR TITLE-SAMPLE FOR

INPUT DATA
TSTART = 0.00 TCIAL = 60.00 HP = .0625 DTPO = 2.00
IGUIDE = 2 IAC = 1 IPLOT = 0 DPLOT = 1.00
IACIT = 0 IACOUT = 1 IEDIT = 0 ISTOP = 1
IPCODE = 1

NUMBER OF COMPONENTS = 12
NUMBER OF CORRELATIONABLE PAIRS = 0
NUMBER OF SATELLITE ELLIPSOIDS = 0
NUMBER OF BLAST ELLIPSOIDS = 1
NUMBER OF DIRECT-HIT-NO-KILL ELLIPSOIDS = 8
NUMBER OF DIRECT-HIT-WITH-KILL ELLIPSOIDS = 6
NUMBER OF CLUTTER POINTS = 23
NUMBER OF KILL LEVELS = 2
NUMBER OF FRAGMENT WEIGHT CLASSES = 1

COMPONENT LOCATIONS

	X	Y	Z
1	-4.70	0.00	4.70
2	-4.10	0.00	1.40
3	-29.10	0.00	1.40
4	-17.90	1.90	3.50
5	-17.90	-1.90	3.50
6	-23.50	1.90	3.60
7	-23.50	-1.90	3.60
8	-24.20	0.00	3.10
9	-23.20	6.60	5.60
10	-23.20	-4.60	5.60
11	-35.30	0.00	3.70
12	-32.30	0.00	3.70

BLAST ELLIPSOIDS

CENTROIDS AND SEMI-AXES

	X	Y	Z	A	B	C
1	-23.40	0.00	5.00	35.64	40.09	35.64

DIRECT-HIT-NO-KILL ELLIPSOIDS

CENTROIDS AND SEMI-AXES

	X	Y	Z	A	B	C
1	-23.10	0.00	5.00	23.10	3.00	4.00
2	-41.60	0.00	11.10	3.00	.20	3.80
3	-44.40	0.00	15.30	2.80	.13	2.80
4	-25.50	0.00	5.40	4.70	4.70	.50
5	-25.50	-6.80	5.40	4.70	4.70	.50
6	-29.30	15.30	5.40	4.00	4.00	.30
7	-29.30	-15.30	5.40	4.00	4.00	.30
8	-40.80	0.00	3.30	4.30	8.33	.29

DIRECT-HIT-WITH-KILL ELLIPSOIDS

CENTROIDS AND SEMI-AXES

	X	Y	Z	A	B	C
1	-23.10	0.00	5.00	23.10	3.00	4.00
2	-41.60	0.00	11.10	3.00	.20	3.80
3	-44.40	0.00	15.30	2.80	.13	2.80
4	-25.50	0.00	5.40	4.70	4.70	.50
5	-25.50	-6.80	5.40	4.70	4.70	.50
6	-29.30	15.30	5.40	4.00	4.00	.30
7	-29.30	-15.30	5.40	4.00	4.00	.30
8	-40.80	0.00	3.30	4.30	8.33	.20

GUTTER POINT LOCATIONS

	X	Y	Z
1	-4.38	1.70	2.50
2	-3.34	-1.70	2.50
3	-4.00	0.00	6.30
4	-31.50	19.60	7.60
5	-31.50	-19.60	7.60
6	-15.00	2.33	7.20
7	-15.90	-2.33	7.20
8	-30.14	2.20	7.60
9	-20.10	-2.20	7.60
10	-32.80	0.00	9.70
11	-46.20	0.00	7.50
12	-43.40	0.00	18.06
13	-40.50	8.83	6.20
14	-40.50	-8.83	6.20
15	-36.30	2.33	5.30
16	-36.30	-2.33	5.30
17	-43.70	2.00	5.30
18	-43.70	-2.00	5.30
19	-3.20	0.00	6.50
20	-10.00	0.00	8.60
21	-8.83	0.00	5.00
22	-19.00	0.00	1.60
23	-32.00	0.00	2.10

STATIC FRAGMENT DENSITY BY 10 DEGREE INTERVALS

	0	10	20	30	40	50	60	70	80	90	100	110	120	130	140	150	160	170	180
0.	0.	0.	0.	0.	0.	0.	0.	0.	1244.	1228.	1244.	0.	0.	0.	3.	0.	0.	0.	0.

FRAGMENT DISTRIBUTION BY HEIGHT AVERAGE HEIGHT FRACTION OF IN CHAINS ALL FRAGMENTS

145.0 1.00

HALF-ANGLE OF CADAF FUZE = 72.0 DEGREES
 MAXIMUM RANGE OF CADAF FUZE = 200. FEET
 DELAY TIME OF CADAF FUZE = 0.000 SECONDS
 DELAY PROBABILITY OF CADAF FUZE = 0.000
 DELAY TIME OF CONTACT FUZE = 0.000 SECONDS
 DELAY PROBABILITY OF CONTACT FUZE = 0.000
 NORMALIZING SPEED FOR VULNERABLE AREA TABLE = 5000. FPS.
 MISS ASSUMED AFTER FAILURE TO FUZE WHEN RANGE = 800. FEET
 FRAGMENT FRAG. COEFFICIENT = 0.0200
 FRAGMENT VELOCITY COEFF. = 0.700. FPS.

*****MISSILE TYPE 2*****

LIST OF EXTR

J	EXTEND	
1	1.000000E+03	NEVER BEGIN MANEUVER
24	2.000000E+00	TIME BETWEEN MISSILES (SEC)
25	1.000000E+03	NEVER FIRE SECOND SALVO
41	1.000000E+05	MAXIMUM LAUNCH RANGE (FT)
42	0.	MINIMUM LAUNCH RANGE (FT)
43	5.000000E+04	MAX ALTITUDE FOR LAUNCH (FT)
44	0.	MIN TARGET ALTITUDE (FT)
48	9.000000E+01	MAX LAUNCH ELEVATION (DEG)
49	0.	MIN TARGET ELEVATION (DEG)
53	1.200000E+04	GUIDANCE GAIN
54	1.500000E+04	RANGE FROM MISSILE TO A/C BEGIN HOMING (FT)
55	6.000000E+01	FRONT VULNERABLE AREA (SQ FT)
56	6.000000E+02	REAR VUL AREA (SQ FT)
57	1.000000E+02	SIDE VUL AREA (SQ FT)
58	6.020000E+03	BOTTOM VUL AREA (SQ FT)
59	3.000000E-03	TRACKING ERROR (RAD)
60	2.000000E+01	ERROR FOR HOMING GUIDANCE (FT)

LIST OF EXTR

J	EXTEND	
11	2	= MISSILES IN SALVO
12	2	= SALVOS
13	1	DO NOT DETECT OR ACQUIRE
20	20	= MISSILES ALLOWED IN AIR
26	0	SUPPRESS ANGULAR RATE TEST
27	0	SUPPRESS SPP & CLOSING TEST

INITIAL AIRCRAFT STATE VECTOR

POSITION	-2.50000E+04	0.	5.00000E+03
VELOCITY	2.54951E+04	3.14159E+00	1.97395E-01
	5.00000E+02	0.	0.
	5.00000E+02	0.	0.

ALTITUDE OF SAM SITE 0. FT. STRUCTURE LIMIT 2.0 G'S THROTTLE SETTING .30
 NUMBER OF TIME LAGS 1 TIME LAGS IN SEC. .100

*****-93 IS A/C AERO TABLE*****

TIME= 0.000 A/C FLAG= 1 1 1 SANSITE FLAG= 1 1 1

AIRCRAFT VARIABLES

FX	RY	RZ	RMAG	VX	VY	VZ	VMAG
-25000.0	0.0	5000.0	25495.	500.	0.	0.0	500.0
MACH	ALPHA	GFORCE	THRUST	THRUST	LIFT	CL	CD
.40	0.00	0.00	0.	.30	0.	0.000	0.000
ACOM	ACUTA	ACUTD	ACUT	VDOT			
0.0	3.0	0.0	0.0	0.0			

*****MISSILE NO. 1 (BODY NO. 1) IS LAUNCHED AT TIME = 0.000

TIME= 0.000 A/C FLAG= 1 1 1 SANSITE FLAG= 4 0 0

AIRCRAFT VARIABLES

FX	RY	RZ	RMAG	VX	VY	VZ	VMAG
-25000.0	0.0	5000.0	25495.	500.	0.	0.0	500.0
MACH	ALPHA	GFORCE	THRUST	THRUST	LIFT	CL	CD
.40	0.00	0.00	0.	.30	0.	0.000	0.000
ACOM	ACUTA	ACUTD	ACUT	VDOT			
0.0	3.0	0.0	0.0	0.0			

MISSILE OUTPUT

NO.	X	Y	Z	VX	VY	VZ	VMAG	MACH	PREL	KDOT	LAMEDAE	LAMEDAA	DELE	DELA
1	0.	0.	0.	-9.1	-9.0	4.2	10.0	0.00	25495.	0.0	0.00	0.00	0.000	0.000

TIME= 2.000 A/L FLAG= 2 1 1 SAMSITE FLAG= 5 1 0

ATCRAFT VARIABLES STATE

PX	RY	RZ	RHAG	VX	VY	VZ	VHAG
-2399.9	0.0	5000.0	24515.	500.	0.	0.0	500.1
MALE	ALPHA	GFORCE	THRUST	THRUST	DRAG	CL	CO
.46	5.30	1.00	5493.	.30	5429.	.294	.040
ACOM	ACUTA	ACUTD	ADOT	VDOT			
0.0	0.0	0.0	0.0	.0			

MISSILE OUTPUT

MO.	X	Y	Z	VX	VY	VZ	VHAG	MACH	RREL	PDOT	LAMBDAE	LAMBDAE	DELE	DELA
1	-769.	-6.	259.	-797.0	-0	237.2	831.5	.72	23710.	1318.3	0.00	0.00	0.000	0.000

TIME= 4.000 A/L FLAG= 2 1 1 SAMSITE FLAG= 5 1 0

ATCRAFT VARIABLES STATE

PX	RY	RZ	RHAG	VX	VY	VZ	VHAG
-2299.7	0.0	5000.0	23537.	500.	0.	0.0	500.1
MALE	ALPHA	GFORCE	THRUST	THRUST	DRAG	CL	CO
.46	5.30	1.00	5494.	.30	5429.	.294	.040
ACOM	ACUTA	ACUTD	ADOT	VDOT			
0.0	0.0	0.0	0.0	.0			

MISSILE OUTPUT

MO.	X	Y	Z	VX	VY	VZ	VHAG	MACH	RREL	PDOT	LAMBDAE	LAMBDAE	DELE	DELA
1	-3258.	-0.	917.	-1704.9	-0	416.2	1755.0	1.55	20159.	2243.7	0.00	0.00	0.000	0.000

*****MISSILE NO. 2 BODY NO. 20 IS LAUNCHED AT TIME = 5.000

TIME= 5.000 A/C FLAGS- 2 1 1 SAMSITE FLAGS- 4 1 0

AIRCRAFT VARIABLES STREFT

FX	RY	RZ	RPAG	VX	VY	VZ	VMAG	
-22499.6	0.0	5000.0	23000.	500.	0.	0.0	500.2	
PACH	ALPHA	GFORCE	THRUST	THRCTL	LIFT	CL	CD	CLMX
.46	5.30	1.00	5494.	.30	40004.	.294	.040	.970
ACCH	ACUTA	ACUTE	ADOT	VDOT				
0.0	0.0	0.0	0.0	.0				

MISSILE OUTPUT

NO.	X	Y	Z	VX	VY	VZ	VMAG	MACH	PREL	ROOT	LAMBDAE	LAMBDAA	DELE	DELA
1	-5103.	-0.	1351.	-1482.1	-0	426.7	1929.9	1.74	17775.	2419.2	0.00	0.00	0.000	0.000
2	0.	0.	0.	-9.0	-0	4.4	10.0	0.00	23048.	0.0	0.00	0.00	0.000	0.000

TIME= 6.000 A/C FLAGS- 2 1 1 SAMSITE FLAGS- 5 2 0

AIRCRAFT VARIABLES STREFT

FX	RY	PZ	RPAG	VX	VY	VZ	VMAG	
-21999.4	0.0	5000.0	22500.	500.	0.	0.0	500.2	
PACH	ALPHA	GFORCE	THRUST	THRCTL	LIFT	CL	CD	CLMX
.46	5.30	1.00	5494.	.30	40004.	.294	.040	.970
ACCH	ACUTA	ACUTE	ADOT	VDOT				
0.0	0.0	0.0	0.0	.0				

MISSILE OUTPUT

NO.	X	Y	Z	VX	VY	VZ	VMAG	MACH	PREL	ROOT	LAMBDAE	LAMBDAA	DELE	DELA
1	-6956.	-0.	1764.	-1907.3	-0	399.2	1944.7	1.75	15349.	2433.6	0.00	0.00	0.000	0.000
2	-192.	-0.	75.	-374.0	-0	140.9	400.4	.34	22366.	884.5	0.00	0.00	0.000	0.000

TIME= 8.000 A/C FLAGS- 2 1 1 SAMSITE FLAGS- 5 2 0

AIRCRAFT VARIABLES SIREFLY

RX	PY	PZ	RHAG	VX	VY	VZ	VMAG
-20509.0	0.0	5000.0	21586.	500.	0.	0.0	500.3
MACH	ALPHA	GEORGE	THRUST	LIFT	URAG	CL	CD
.46	5.53	1.00	5494.	40004.	5430.	.234	.040
ACOM	AOITA	AOUID	AOUT	VOOT			
0.0	0.0	0.0	0.0	.0			

MISSILE OUTPUT

NO.	X	Y	Z	VX	VY	VZ	VMAG	MACH	RREL	RUOT	LAMBDAE	LAMBDAI	LAMBDAJ	DELE	DELA
1	-10843.	0.	2023.	-1940.0	.0	375.6	1976.0	1.78	10455.	2459.7	.00	240.32	.00	0.00	-0.00
2	-1773.	-0.	578.	-1233.4	-0.	554.6	1283.3	1.13	19726.	1769.0	0.00	0.00	0.00	0.00	0.00

TIME= 10.000 A/C FLAGS- 2 1 1 SAMSITE FLAGS- 5 2 0

AIRCRAFT VARIABLES SIREFLY

RX	PY	PZ	RHAG	VX	VY	VZ	VMAG
-19998.4	0.0	5000.0	20614.	500.	0.	0.0	500.3
MACH	ALPHA	GEORGE	THRUST	LIFT	DRAG	CL	CD
.46	5.29	1.00	5494.	40004.	5431.	.234	.040
ACOM	AOITA	AOUID	AOUT	VOOT			
0.0	0.0	0.0	0.0	.0			

MISSILE OUTPUT

NO.	X	Y	Z	VX	VY	VZ	VMAG	MACH	RREL	RUOT	LAMBDAE	LAMBDAI	LAMBDAJ	DELE	DELA
1	-14741.	0.	3328.	-1952.5	.0	453.9	2004.6	1.82	5516.	2475.0	654.86	.00	0.00	-1.707	-0.00
2	-5068.	-0.	1451.	-1870.6	-0.	464.0	1927.3	1.73	15346.	2410.0	0.00	0.00	0.00	0.00	0.00

*****MISSILE NO. 3 BODY NO. 3) IS LAUNCHED AT TIME = 19.000

TIME = 19.000 A/C FLAGS- 2 1 1 SANSITE FLAGS- 4 2 0

AIRCRAFT VARIABLES STRELT

FX	KV	RZ	FMAG	VX	VY	VZ	VMAG
-13598.4	0.0	5000.0	20614.	500.	0.	0.0	500.3
MACH	ALPHA	GFORCE	THRUST	THRUST	LIFT	CL	CLMX
.46	5.29	1.00	5494.	.30	40004.	.294	.040 .979
ACOM	AOUTA	ACOUTD	AOUT	VDOT			
0.0	0.0	0.0	0.0	.0			

MISSILE OUTPUT

NO.	X	Y	Z	VX	VY	VZ	VMAG	MACH	RREL	FOOT	LAMBDAE	LAMBDAA	DELE	DELA
1	-14761.	0.	3328.	-1952.5	.0	453.9	2004.6	1.02	5516.	2475.0	654.86	.00	-1.707	-0.00
2	-5068.	-0.	1451.	-1870.6	-0.	464.0	1927.3	1.73	15346.	2414.0	0.00	0.00	0.009	0.000
3	0.	0.	0.	-8.9	-0.	4.6	10.0	0.00	20614.	0.0	0.00	0.00	0.000	0.000

LAST MISSILE IN SALVO FIRED AT TIME = 10.000

TIME = 12.000 A/C FLAGS- 2 1 1 SANSITE FLAGS- 6 3 0

AIRCRAFT VARIABLES STRELT

FX	KV	RZ	FMAG	VX	VY	VZ	VMAG
-18397.7	0.0	5000.0	19645.	500.	0.	0.0	500.4
MACH	ALPHA	GFORCE	THRUST	THRUST	LIFT	CL	CLMX
.46	5.29	1.00	5494.	.20	40004.	.294	.040 .979
ACOM	AOUTA	ACOUTD	AOUT	VDOT			
0.0	0.0	0.0	0.0	.0			

MISSILE OUTPUT

NO.	X	Y	Z	VX	VY	VZ	VMAG	MACH	RREL	FOOT	LAMBDAE	LAMBDAA	DELE	DELA
1	-18525.	0.	4569.	-1675.1	-0.	935.8	1910.8	1.76	639.	2238.2	10846.87	.00	-10.000	-0.00
2	-3857.	-0.	2325.	-1913.8	-0.	409.7	1957.2	1.77	10492.	2438.8	242.36	.00	0.000	0.000
3	-754.	-0.	291.	-783.2	-0.	271.7	829.0	.72	18841.	1310.7	0.00	0.00	0.000	0.000

SUMMARY OF KILL DUE TO MISSILE NO. 1

***MISSILE NO. 1 BURSTS DUE TO PACAP FUZE AT TIME= 12.270 AND RANGE= 191.0 FEET

STATE VECTORS IN INERTIAL COORDINATES AT BURST

	X	Y	Z	VX	VY	VZ
AIRCRAFT -14462.		0.	500.	500.4	0.0	0.0
MISSILE -14463.		0.	488.	-1547.5	-0.0	1089.9

MISSILE IN A/C BODY COORDINATES

	X	Y	Z	ELEVATION	AZIMUTH
-115.15		0.0	-152.42	-52.93	180.00

A/C IN MISSILE BODY COORDINATES

	X	Y	Z	ELEVATION	AZIMUTH
58.46		-0.00	-182.50	72.61	0.00

MISSILE STATUS AT BURST

COMPONENT	DEL	ANY	AP
7.724E-10	-2.430E+02	-5.528E+02	-1.000E+01
7.655E-33	6.190E-07	-8.773E-08	-5.757E-09
-3.28E-10	8.60E+02		2.092E-09

KILL LEVEL 1

COMPONENT	SINGLE-SHOT SURVIVAL PROBABILITY	CUMULATIVE SURVIVAL PROBABILITY
1	.996	.996
2	1.000	1.000
3	1.000	1.000
4	1.000	1.000
5	1.000	1.000
6	1.000	1.000
7	1.000	1.000
8	1.000	1.000
9	1.000	1.000
10	1.000	1.000
11	1.000	1.000
12	1.000	1.000

KILL LEVEL 2

COMPONENT	SINGLE-SHOT SURVIVAL PROBABILITY	CUMULATIVE SURVIVAL PROBABILITY
1	.989	.989
2	.999	.999
3	.955	.955
4	.950	.950
5	.950	.950
6	.967	.967
7	.967	.967
8	.903	.903
9	.966	.966
10	.966	.966
11	.996	.996
12	.994	.994

KILL LEVEL 1

COMPONENT	SINGLE-SHOT SURVIVAL PROBABILITY	CUMULATIVE SURVIVAL PROBABILITY
1	.996	.996
2	1.000	1.000
3	1.000	1.000
4	1.000	1.000
5	1.000	1.000
6	1.000	1.000
7	1.000	1.000
8	1.000	1.000
9	1.000	1.000
10	1.000	1.000
11	1.000	1.000
12	1.000	1.000

KILL LEVEL 2

COMPONENT	SINGLE-SHOT SURVIVAL PROBABILITY	CUMULATIVE SURVIVAL PROBABILITY
1	.989	.989
2	.999	.999
3	.955	.955
4	.950	.950
5	.950	.950
6	.967	.967
7	.967	.967
8	.903	.903
9	.966	.966
10	.966	.966
11	.996	.996
12	.994	.994

TIME= 14.000 A/C FLAG= 2 1 1 SAMSITE FLAG= 6 3 0

AIRCRAFT VARIABLES STRFLT

RV	RY	RZ	RHAG	VX	VY	VZ	VHAG
-17395.8	0.0	5000.0	18679.	500.	0.	0.0	500.4
MACH	ALPHA	GFORCE	THRUST	LIFT	DRAG	CL	CD
.46	5.29	1.00	5494.	40004.	5432.	.294	.040
ACOM	ACUTA	ACUTO	ADOT				
0.0	0.0	0.0	0.0				

MISSILE OUTPUT

NO.	X	Y	Z	VX	VY	VZ	VHAG	MACH	PREL	ROOT	LAMBDAE	LAMBDAE	DELE	DELA
2	-17397.	0.	3199.	-1922.8	0.	490.4	1984.4	1.80	5598.	2452.2	656.01	0.00	-1.819	-0.000
3	-17365.	-0.	1059.	-1679.7	-0.	491.4	1750.1	1.55	15308.	2233.1	0.00	0.00	0.000	0.000

TIME= 16.000 A/C FLAG= 2 1 1 SAMSITE FLAG= 6 3 0

AIRCRAFT VARIABLES STRFLT

RV	RY	RZ	RHAG	VX	VY	VZ	VHAG
-16594.9	0.0	5000.0	17716.	501.	0.	0.0	500.5
MACH	ALPHA	GFORCE	THRUST	LIFT	DRAG	CL	CD
.46	5.29	1.00	5494.	40004.	5432.	.294	.040
ACOM	ACUTA	ACUTO	ADOT				
0.0	0.0	0.0	0.0				

MISSILE OUTPUT

NO.	X	Y	Z	VX	VY	VZ	VHAG	MACH	KREL	ROOT	LAMBDAE	LAMBDAE	DELE	DELA
2	-1641E.	0.	4539.	-1648.9	-0.	955.4	1905.7	1.75	760.	2257.6	8299.33	0.00	-10.000	-0.000
3	-16498.	-0.	2071.	-1876.8	-0.	483.6	1919.1	1.75	10523.	2418.0	0.00	0.00	0.000	0.000

SUMMARY OF KILL DUE TO MISSILE NO. 2

*****MISSILE NO. 2 ENDS DUE TO RADAR FUZZ AT TIME = 16.730 AND RANGE = 107.8 FEET

STATE VECTORS IN INERTIAL COORDINATES AT BURST

	X	Y	Z	VX	VY	VZ
AIRCRAFT	-16831.	0.	5000.	500.5	0.0	0.0
MISSILE	-16938.	0.	4845.	-1495.1	-0.	1106.4

MISSILE IN A/C BODY COORDINATES

X	Y	Z	ELEVATION	AZIMUTH
-120.46	.00	-144.10	-50.11	180.00

A/C IN MISSILE BODY COORDINATES

X	Y	Z	ELEVATION	AZIMUTH
55.23	-0.00	-179.52	72.91	.00

MISSILE STATUS AT RUSSI

CMFG	AMI	ANY	DEL	AB
3.75E-10	-3.79E+02	-5.771E+02	-1.00E+01	1.519E+01
8.18E-01	5.796E-07	-8.150E-08	-5.615E-03	1.375E-09
-1.01E-10	8.84E+02			

CONCURRENT NUMBER	KILL LEVEL 1		KILL LEVEL 2	
	SINGLE-SHOT SURVIVAL PROBABILITY	CUMULATIVE SURVIVAL PROBABILITY	SINGLE-SHOT SURVIVAL PROBABILITY	CUMULATIVE SURVIVAL PROBABILITY
1	.992	.988	.974	.963
2	1.000	1.000	.997	.996
3	1.000	1.000	.989	.989
4	1.000	1.000	.981	.987
5	1.000	1.000	.979	.985
6	1.000	1.000	.917	.987
7	1.000	1.000	.915	.985
8	1.000	1.000	.752	.979
9	1.000	1.000	.914	.983
10	1.000	1.000	.914	.983
11	1.000	1.000	.987	.983
12	1.000	1.000	.981	.975

	KILL LEVEL 1		KILL LEVEL 2
AIRCRAFT	AIRCRAFT	AIRCRAFT	AIRCRAFT
SINGLE-SHOT	CUMULATIVE	SINGLE-SHOT	CUMULATIVE
KILL	KILL	KILL	KILL
PROBABILITY	PROBABILITY	PROBABILITY	PROBABILITY
=	=	=	=
.009	.067	.468	.777

TIME= 18.000 A/C FLAGS- 2 1 1 SAMSITE FLAGS- 6 3 0

AIRCRAFT VARIABLES

PX -15996.8 RY 0.0 RZ 5000.0 PHAG 11758. VX 501. VY 0. VZ 0.0 VHAG 500.6
 MACH .46 ALPHA 5.29 GFORCE 1.00 THRUST 5494. THROTL .30 LIFT 40005. CL .294 CO .040 CLMX .970
 ACOM 0.0 ACUTA 0.0 ADUT 0.0 VDOT .0

MISSILE OUTPUT

NO. 3 -10576. Y 0. Z 3021. -1894.7 VX 0. VY 519.1 VMAG 1964.5 MACH 1.78 RRFL 5675. RDOT 2425.9
 LAMEDAA .00 -1.950 DELE -0.000
 LAMEDAE 716.02
 LAMEDAA DELE DELE

TIME= 20.000 A/C FLAGS- 2 1 1 SAMSITE FLAGS- 6 3 0

AIRCRAFT VARIABLES

PX -14993.6 RY 0.0 RZ 5000.0 PHAG 11805. VX 501. VY 0. VZ 0.0 VHAG 500.6
 MACH .46 ALPHA 5.29 GFORCE 1.00 THRUST 5494. THROTL .30 LIFT 40005. CL .294 CO .040 CLMX .970
 ACOM 0.0 ACUTA 0.0 ADUT 0.0 VDOT .0

MISSILE OUTPUT

NO. 3 -14316. Y 0. Z 4469. -1597.8 VX 0. VY 937.7 VMAG 1881.1 MACH 1.72 RRFL 900. RDOT 2234.1
 LAMEDAA .00 -10.000 DELE -0.000
 LAMEDAE 7014.60
 LAMEDAA DELE DELE

SUMMARY OF KILL DUE TO MISSILE NO. 3

*****MISSILE NO. 3 BURSTS DUE TO RADAR FUZE AT TIME = 27.402 AND RANGE = 209.2 FEET

STATE VECTORS IN INERTIAL COORDINATES AT BURST

	X	Y	Z	VX	VY	VZ
AIRCRAFT	-14792.	0.	5000.	500.6	0.0	0.0
MISSILE	-14926.	0.	4839.	-1416.4	-0	1154.8

MISSILE IN AZC BODY COORDINATES

	X	Y	Z	ELEVATION	AZIMUTH
	-147.66	.90	-148.14	-45.09	180.00

AZC IN MISSILE BODY COORDINATES

	X	Y	Z	ELEVATION	AZIMUTH
	53.85	-0.00	-209.43	73.38	.00

MISSILE STATUS AT BURST

	DEL	AB
2.058E-10	-7.669E+02	-1.000E+01
6.832E-01	4.034E-17	-4.530E-09
-2.00E-10	6.03E+02	1.523E-09

COMPONENT NUMBER	KILL LEVEL 1		KILL LEVEL 2	
	SINGLE-SHOT SURVIVAL PROBABILITY	CUMULATIVE SURVIVAL PROBABILITY	SINGLE-SHOT SURVIVAL PROBABILITY	CUMULATIVE SURVIVAL PROBABILITY
1	.989	.977	.966	.931
2	1.000	1.000	.996	.992
3	1.000	1.000	.937	.711
4	1.000	1.000	.876	.699
5	1.000	1.000	.834	.697
6	1.000	1.000	.881	.781
7	1.000	1.000	.890	.779
8	1.000	1.000	.842	.636
9	1.000	1.000	.881	.778
10	1.000	1.000	.881	.778
11	1.000	1.000	.379	.962
12	1.000	1.000	.970	.965

KILL LEVEL 1		KILL LEVEL 2	
AIRCRAFT SINGLE-SHOT KILL PROBABILITY	AIRCRAFT CUMULATIVE KILL PROBABILITY	AIRCRAFT SINGLE-SHOT KILL PROBABILITY	AIRCRAFT CUMULATIVE KILL PROBABILITY
.611	.023	.794	.953

SALVO NO. 1 COMPLETE AT TIME = 20.438
NEXT SALVO BEGINS AT TIME = 1020.438

SECTION 4
PROGRAM LISTINGS

The following pages of this section are the FORTRAN program listings for those portions of the DSAMAM program which have been modified for the endgame. This includes the main program, subroutine MISSILE, and the following new subroutines:

- . SPRAY
- . STAB
- . CONFUZE

```

1      PROGRAM (VNCAM)INPUT,OUTPUT=7137,TAPE1,TAPE2,TAPE3,TAPE10,
2      COMMON/DRIVE/ TIME,MM,ISTART,ISTOP,EXTF(60),TEXT(30),TITLE(10),
3      SEG,6,PI,RAD
4      COMMON/FLAS/JFOL,KPOL,LFOL,JFSAM,KFSAM,LEAM,NMIN,ISTOP,IAC,IEDIT,
5      IGUIDE,IPROCE,MEIAC(20),JV
6      COMMON/ATACF/FA(6),VA(6),ACOMA,ACOMD,ACOM,ACUTA,AOUTD,AOUT,VOUT,
7      UUTIV(3),A(3),C(3),UNIT(1),A1(3),D1(3),HACH,OA,
8      ALPHA,LTHT,DEAG,GFGECE,UNITL(3),CL,CG,CLMX,SA,CA,
9      THROST,THROIL,ASMAX,ACTION,PASMX,DUMPL,DUMCL,ITAU,
10     TAU(2),ADD(2,2)
11     COMMON/ACATA/TAUT(13,21),COC(21),CCCL(21),PACHMX(13),ALPHA0(21)
12     ,DALUCL(1),CLMAX(21),AREA,WEIGHT
13     COMMON/MISCL/FM(6,20),VM(6,20),MACPM(20),QAP(20),SSA,AREAN,
14     VV(2,20),DEL(2,20),A1(2,20),H1(20),RAM(20),KAMD(20)
15     COMMON/PFTN/TA,TAJX
16     COMMON/COE/ NCOWS,REVS,NHIS,NHLD5,NHLAST,NGL17,THA,RCHA,VE,
17     IDLT,XCM,XCP,ZCP,VNE,THI,I
18     COMMON /THO/ XGL(25),YGL(25),ZGL(25),XSH(25),YSH(25),ZSH(25),
19     LASH(25),BSH(25),GSH(25),XBL(25),YBL(25),ZBL(25),XBL(25),YBL(25),
20     ZBL(25),XCNCL(20),YCNCL(20),ZCNCL(20),EX(25),MY(25),ZEL(25),
21     ZTAN(9),TMT(9)
22     COMMON /THREE/ NUOHL,NHNRK,NDRK,NAFAR,KHAY,DIRE,PORE,DICE,PUCF,
23     IRMISS,CDE
24     COMMON /FOUR/ X0(25,2),Y0(25,2),Z0(25,2),XS(25,2),YS(25,2),
25     ZS(25,2),WATE(10)
26     COMMON /FIVE/ VOL(2,11,72),STEAR(19),FRAC(10),SLUM(10)
27     COMMON /SIX/ CPS(4,25)
28     DIMENSION THEC(19)
29     REAL LIFT,MACH,MACHM,MACHMX
30     INTEGER AFLACS(6)
31     EQUIVALENCE (AFLACS(1),JFOL)
32     REAL SVST(12),VPAPM(13,20)
33     REAL XAIF(16),XAIR(21367)
34     EQUIVALENCE (XAIF(1),TOLIR(1,1)), (XAIR(2),TALTR(7,1))
35     INTEGER JX(3),ICODE(2)
36     REAL PAPHM(13,3),ORANE(6),ZMOR(4)
37     INTEGER IPARM(3),JPARM(3)
38     LOGICAL IPU(8)
39     EQUIVALENCE (JX(1),JD), (JX(2),J2), (JX(3),J3), (ZMOR(1),ACTION)
40     DATA "LANK/IN /
41     DATA CO/THO/
42     DATA FND/AM/END/, ACOM/AM/END/
43     NAMELIST/INPUT/TOTAL,MM,ISTART,UTFO,ICORD,TCUJOF,IPRINT,IAC,
44     IPLOT,DPLOT,IACIN,IACOUT,IEDIT,ISTOP,IMODE
45     C***** INITIALIZE CONSTANTS
46     DEU=57.29578
47     G=32.174
48     PI=ATAN2(0.,-1.)
49     RAD=1.745329E-02
50     A(3)=6.
51     C***** 700 EXTRA VARIABLES

```

PROGRAM	74/74	OPT=1	FIN 4.64420	77/08/04.	14.10.44	PAGE 2
---------	-------	-------	-------------	-----------	----------	--------

```

55 DO 50 J=1,20
56   EXTR(J)=0.
57   EXTR(J,30)=0.
58   50 IFEXTR(J)=0
59   C*****INITIALIZE NAMELIST FLAGS
60   IPLOT=0
61   ISTART=0.
62   IACIN=0
63   IASTOR=0
64   IACOUT=0
65   IFOUT=0
66   IPRINT=1
67   IAC=1
68   IGUIOF=1
69   ICODE=1
70   ICODE(1)=1
71   ICODE(2)=1
72   C*****FAD NAMELIST, COMMENT, AND TITLE
73   100 READ(5,INPUT)
74   IF(TOTAL,LT,0.) GO TO 1000
75   C*****Set STORAGE FLAG IF TRAJECTORY OUTPUT IS DESIRED
76   IF(IACOUT,GT,0) ISIOR=1
77   WRITE(6,F000)
78   600 FORMAT(1H1)
79   101 READ(5,500) TITLE
80   500 FORMAT(18A4)
81   IF(TITLE(1).NE.'GO') GO TO 103
82   WRITE(6,601) TITLE
83   601 FORMAT(1Y,18A4)
84   GO TO 101
85   103 WRITE(6,602) TITLE
86   602 FORMAT(1H0,18A4/)
87   WRITE(6,F03) ISTART,IMODE
88   1
89   603 FORMAT(11H0INPUT DATA/3H ISTART=,F7.2,10H TOTAL=,F9.2,3X,
90     1 3HIME=,F7.4,2X,6HCTPO=,F6.2,5X,8HIGUIDE=,I3,3X,
91     2 5HIAL=,I3,3X,7H1PLOT=,I3,2X,7HCPLOT=,F7.2,5X,
92     3 7HACIN=,I3,4X,8H1ACOUT=,I3,3X,7H1EDIT=,I3,3X,
93     4 7H1STOR=,I3,5X,7H1MODE=,I3)
94   C*****READ CONTROL PARAMETERS
95   READ(5,2000)INCOMP3,NDUBLY,NSHLD5,NBLAST,NDHNRK,NDHK,MGLIT,NLEVS,
96     1NMTS
97   2000 FORMAT(9I3X,12I)
98   WRITE(6,3000)NCORPS,NDUBLY,NSHLD5,NBLAST,NDHNRK,NDHK,MGLIT,NLEVS,
99     1NMTS
100   3000 FORMAT(11H1" NUMBER OF COMPONENTS",22X,"=",I3/
101     1" NUMBER OF DOUBLY VULNERABLE PAIRS",9X,"=",I3/
102     2" NUMBER OF SHIELDING ELLIPSOIDS",12X,"=",I3/
103     3" NUMBER OF BLAST ELLIPSOIDS",16X,"=",I3/
104     4" NUMBER OF DIRECT-HIT-NC-KILL ELLIPSOIDS "=",I3/
105     5" NUMBER OF DIRECT-HIT-MVM-KILL ELLIPSOIDS "=",I3/
106     6" NUMBER OF GLITTER POINTS",16X,"=",I3/
107     7" NUMBER OF KILL LEVELS",21X,"=",I3/

```


PROGRAM	LYNSAM	74/74	OPT=1	FIN 4.6.4.20	77/04/04, 14.10.44	PAGE
110	C*****	NUMBER OF FRAGMENT WEIGHT CLASSES",9X,"=",13)				30
	READ COMPONENT LOCATIONS					31
	READ(15,2001)(X(K),Y(K),Z(E(K),K=1,NCOMP)					32
	2001 FORMAT(3F10.0)					33
	WRITE(16,3001)					34
	2001 FORMAT(//16X,"COMPONENT LOCATIONS")					35
	WRITE(16,3002)(K,X(K),Y(K),Z(E(K),K=1,NCOMP)					36
	3002 FORMAT(19X,"X",14X,"Y",14X,"Z",5X,"Z(E(K),K=1,NCOMP)					37
115	C*****	READ SHIELD ELLIPSOID LOCATIONS AND SEMIAXES				38
	IF(NSHLDS.LT.1) GO TO 800					39
	READ(15,2002)(XSH(K),YSH(K),ZSH(K),ASH(K),BSH(K),K=1,NSHLDS)					40
	2002 FORMAT(6F10.0)					41
	WRITE(16,3003)					42
120	2003 FORMAT("1",33X,"FRAGMENT SHIELDING ELLIPSOIDS")					43
	WRITE(16,3004)(K,XSH(K),YSH(K),ZSH(K),ASH(K),BSH(K),CSH(K),					44
	1K=1,NSHLDS)					45
	2004 FORMAT(17X,"CENTROIDS AND SEMI-AXES"/19X,"X",14X,"Y",14X,"Z",					46
	11A",14X,"R",14X,"C",5X,"Z(E(K),K=1,NCOMP)					47
125	C*****	READ ELAST ELLIPSOID LOCATIONS AND SEMIAXES				48
	IF(NPLAST.LT.1) GO TO 801					49
	READ(15,2005)(XBL(K),YBL(K),ZBL(K),ABL(K),BBL(K),CBL(K),K=1,NBLAST)					50
	2005 FORMAT("1",39X,"BLAST ELLIPSOIDS")					51
	WRITE(16,3006)(K,XBL(K),YBL(K),ZBL(K),ABL(K),BBL(K),CBL(K),					52
	1K=1,NBLAST)					53
130	C*****	READ DIRECT-HIT-NO-KILL ELLIPSOID LOCATIONS AND SEMIAXES				54
	IF(NDHKK.LT.1) GO TO 802					55
	READ(15,2006)(XOK(K),YOK(K),ZOK(K),XSK(K),YSK(K),ZSK(K),					56
	1K=1,NDHKK)					57
135	WRITE(16,3006)					58
	2006 FORMAT(//34X,"DIRECT-HIT-NO-KILL ELLIPSOIDS")					59
	WRITE(16,3007)(K,XOK(K),YOK(K),ZOK(K),XSK(K),YSK(K),ZSK(K),					60
	1K=1,NDHKK)					61
140	C*****	READ DIRECT-HIT-NO-KILL ELLIPSOID LOCATIONS AND SEMIAXES				62
	IF(NDHKK.LT.1) GO TO 802					63
	READ(15,2007)(XOK(K),YOK(K),ZOK(K),XSK(K),YSK(K),ZSK(K),					64
	1K=1,NDHKK)					65
	WRITE(16,3007)					66
145	2007 FORMAT(//32X,"DIRECT-HIT-NO-KILL ELLIPSOIDS")					67
	WRITE(16,3008)(K,XOK(K),YOK(K),ZOK(K),XSK(K),YSK(K),ZSK(K),					68
	1K=1,NDHKK)					69
150	C*****	READ GLITTER POINT LOCATIONS				70
	IF(NDGLTT.LT.1) GO TO 803					71
	READ(15,2008)(XGL(K),YGL(K),ZGL(K),K=1,NDGLTT)					72
	2008 FORMAT(6,3008)					73
	3008 FORMAT("1",13X,"GLITTER POINT LOCATIONS")					74
	WRITE(16,3009)(K,XGL(K),YGL(K),ZGL(K),K=1,NDGLTT)					75
	C*****	READ VULNERABLE AREA TABLES				76
	KIND=C*NCORPS*NMIS					77
	DO 803 LEV=1,NLEVS					78
	DO 803 K=1,KIND					79
	803 READ(15,2009)(VULLEV,J,K),J=1,11)					80
	2009 FORMAT(11F7.0)					81
	C*****	END STATIC FRAGMENT DATA BY 10 DEGREE INTERVALS				82

PAGE 4

77709/04. 14.10.44

FTN 4.6+420

PROGRAM EYDSAN 74/74 OPT=1

```

160 READ(5,2004) STEAR
161 FORMAT(A10.0)
162 DO 804 I=1,19
163   804 INE001=10*(I-1)
164   WRITE(6,3009) INE0, STEAR
165   3009 FORMAT(//4X, "STATIC FRAGMENT DENSITY BY 10 DEGREE INTERVALS"/
166     "0", 1917/1X, 131 " " // 1X, 1917.0)
167   C***** READ FOR EACH MASS CLASS THE FRACTION OF ALL FRAGMENTS BELONGING
168     TO THE CLASS AND THE AVERAGE MASS IN GRAINS
169   C
170   READ(5,2005) (FRACT(KMT), MATE(KMT), KMT=1, NNIS)
171   2005 FORMAT(2F10.0)
172   WRITE(6,3010) (MATE(KMT), FRACT(KMT), KMT=1, NNIS)
173   3010 FORMAT(// " FRAGMENT DISTRIBUTION BY HEIGHT"/
174     " 1" AVERAGE HEIGHT FRACTION CF"/
175     " 2" IN GRAINS ALL FRAGMENTS"/ 1X, 32 " " // (F10.1, F17.2))
176   C***** READ FUZE CONSTANTS
177   READ(5,2006) HAFANG, RHAX, DRF, F0-F, DT0F, P0CF
178   WRITE(6,3011) HAFANG, RHAX, DRF, P0CF, DT0F, P0CF
179   3011 FORMAT(// " HALF-ANGLE OF RADAR FUZE", 2X, " = ", F6.1, " DEGREES"/
180     " 1" MAXIMUM RANGE OF RADAR FUZE", 1X, " = ", F5.0, " FEET"/
181     " 2" DELAY TIME OF RADAR FUZE", 2X, " = ", F6.3, " SECONDS"/
182     " 3" PROBABILITY OF RADAR FUZE", 1X, " = ", F6.3/
183     " 4" DELAY TIME OF CONTACT FUZE", 2X, " = ", F6.3, " SECONDS"/
184     " 5" PROBABILITY OF CONTACT FUZE", 1X, " = ", F6.3)
185   HAFANG=HAFANG*PI/180
186   C***** READ MISCELLANY
187   READ(5,2007) VNEHI, RMIS, COR, VE
188   WRITE(6,3012) VNEHI, RMIS, COR, VE
189   3012 FORMAT(// " HOPALIZING SPEED FOR VULNERABLE AREA TABLE " = ", F7.0,
190     " 1" FPS"/
191     " 2" MISS ASSUMED AFTER FAILURE TO FUZE WHEN RANGE = ", F5.0, " FEET"/
192     " 3" FRAGMENT DRAG COEFFICIENT", 2X, " = ", F8.5/
193     " 5" FRAGMENT EMISSION SPEED", 2X, " = ", F7.0, " FPS."/ "1")
194   C***** COMPUTE CONVENTIONAL CONSTANTS
195   THA=TAN(HAFANG)
196   R0MR=MAXVABS(COS(HAFANG))
197   C***** INITIALIZE CUMULATIVE COMPONENT SURVIVAL PROBABILITIES
198   DO 75 LEV=1, NLEVS
199   DO 75 K=1, NCORPS
200   C***** INITIALIZE MISSILE
201   CALL MISINI(KCOR)
202   C***** READ AND PRINT VARIABLE PARAMETERS
203   DO 105 I=1, 1
204   NPARM=1-1
205   READ(5,503) ENDET, JL, JPARM(1), (CARMH(I,1), J=1, 3), (VARM(I,1),
206     J=1, JL)
207   503 FORMAT(44, 214, 348, 112, 7/16512.70)
208   C***** TEST FOR END OF VARIABLE PARAMETER DATA
209   IF (ENDET .EQ. END) GO TO 106
210   JPARM(1)=JL
211   105 WRITE(6,6051), (CARMH(I,1), J=1, 3), JL, JPARM(1), (VARM(I,1), J=1, JL)
212   6051 FORMAT(// " 12, 2X, 3X, 5X, 16PH0. OF VALUES=13, 5X,

```

PAGE 5

77/08/34. 14.10.44

FIN 4.64420

PROGREF DVB SAN 14/74 OPT=1

```

C*****READ AND PRINT EXTR
100 DO 107 J = 1, 60
    READ(5,505) ENDTST,K,IZ,DNAME
    505 FORMAT(I4,F12.7,6A8)
C*****TEST FOR END OF REAL EXTRA VARIABLE DATA
IF(ENDTST.EQ..END) GO TO 10P
C*****IF THERE IS EXTRA DATA WRITE PRINTOUT HEADER FIRST TIME ONLY
IF(J.EQ..1) WRITE(6,607)
        607 FORMAT(13HOLIST OF EXTR//14H J      EXTR(J))
EXTR(KI)=Z
        107 WRITE(6,608) K,IZ,DNAME
        608 FORMAT(I3,I4,1PE14.7,3X,6A8)
C*****KLEAD AND PRINT IEXTR
        100 DO 109 J = 1, 30
            508 FOMAT(I4,214,6A8)
C*****TEST FOR END OF INTEGER EXTRA VARIABLE DATA
IF(ENDTST.EQ..END) GO TO 110
C*****IF THERE IS ITEXTA DATA WRITE PRINTOUT HEADER FIRST TIME ONLY
IF(J.EQ..1) WRITE(6,609)
        609 FORMAT(14HOLIST OF IEXTR//13H J      IEXTR(J))
IEXTR(KI)=IZ
        109 WRITE(6,610) K,IZ,DNAME
        610 FOMAT(I3,I7,11X,6A8)
C*****TEST TO SEE IF A/C TRAJECTORY IS GENERATED
110 IF(IAC.EQ..2) GO TO 120
C*****READ AND PRINT STORED STATE VECTOR
JA=3*(ICORPD(1))-2
JKA=JA+2
JB=3*(ICORPD(2))+6
JK=JB+2
        101 FOMAT (6E12.6)
C*****CHANGE DEGREES TO RADIANS IF DATA IS IN SPHERICAL COORDINATES
DO 113 I = 1,Z
    IF(ICORPD(1).EQ..1) GO TO 113
        KI=6-I-1
        K2=KI+1
        DO 112 J = KI,K2
            112 SVST(J)=SVST(J)*RAD
        113 CONTINUE
    IF(INPARM.EQ..0) JPARM(1)=0
    DO 10 T=1,NPARM
        IF(JPARM(T),LT..0) GO TO 30
10 CONTINUE
    5 CALL CORPO(SVST(1),ICORPD(1))
    CALL CORPOS(SVST(Z),ICORPD(2))
    WRITE (6,612)
        612 FOMAT (30HINITIAL AIRCRAFT STATE VECTOR)
    WRITE (6,613) SVST
        613 FORMATECV,PH,CSTOTUD,IP,CPIS,PYPR,Y,PPY,X,MMOUECTIV,

```

```

114E15.6/13X,IP4E15.6)
00 20 I=1,NPARN
IF(JPARMT).GE.0) GO TO 20
00 15 K=1,12
15 KAKI=SVST(K)
GO TO 152
+0 CONTINUE
30 READ(5,511) SSA,ASMAX,THROIS,ITAU,TAU
511 FORMAT(3F6.0,11.2F6.0)
WRITE(6,615) SSA,ASMAX, THROIS,ITAU,(TAU(I),I=1,ITAU)
615 FORMAT(21HREAL TITUDE OF SAM SITE,F7.0,4H F1.2X,15HSTRUCTURE LIMIT,
1 F4.1,4H G**5.2X,16HNOITILE SETTING,F5.2/5X,
2 19HNUMBER OF TIME LAGS,I3.5X,17HTIME LAGS IN SEC.,2F8.3)
C*****TEST FOR READING OF A/C AERODYNAMIC DATA
IF(IAC.EQ. 0) GO TO 115
READ(5,512) XAIR1,ACN1,XAIR2
512 FORMAT(6E12.5,6G16E12.5)
C*****TEST TO SEE IF A/C DATA IS PROPERLY LOADED AND IS NEEDED
115 IF(ACN1.NE. END) GO TO 117
C*****A/C DATA IS NOT LOADED WRITE MESSAGE + READ NEW DATA
WRITE(6,620)
620 FORMAT(51H0*****A/C AERODYNAMIC TABLES ARE NOT LOADED AND ARE,
1 14H REQUIRED*****215X,17HGOING TO NEXT RUN )
GO TO 100
C*****PRINT OUT TYPE OF A/C TABLES BEING USED
117 WRITE(6,621) ACN1
622 FORMAT(6H0*****A4,24H IS A/C AERO TABLES*****
GO TO 125
C*****READ A/C TRAJECTORY DISPLACEMENT AND SAM ALTITUDE AND PRINT THEM
120 READ(5,515) DP,SSA
515 FORMAT(4F12.7)
WRITE(6,623) DP,SSA
625 FORMAT(46H0A/C TRAJECTORY IS READ IN AND IS DISPLACED BY/1P3E15.5/
1 21H0ALTITUDE OF SAM SITE ,F7.0)
C*****READ A/C TRAJECTORY IF NEEDED
IF(IACIN.GT. 0) READ(IACIN,700) RUNIO,NPTS,
1 (X(IK,IL),IK=1,3),IAC(IK,IL),IK=1,9),IL=1,NPTS)
700 FORMAT(24G,14/16E13.6)
C*****PRINT TITLE OF NEW A/C DATA
WRITE(6,627) IACIN,NPTS,RUNIO
627 FORMAT(42H0AIRCRAFT TRAJECTORY HAS BEEN READ ON UNIT,I3.5X,
1 9HWHERE ARE ,I4,19H POINTS IN THE DATA/5X,
2 16HNE DATA TO IS ,2F4)
C*****TEST FOR PARAMETER VARIATION
125 IF(JPARM.GT. 0) GO TO 123
C*****WRITE TITLE FOR EDITOR IF NEEDED
IF(EDIT.NE. 0) GO TO 140
WRITE(11,761) TITLE
761 FORMAT(4H 1 ,18A4)
JV=0
GO TO 140
C*****INITIALIZE PARAMETER VARIATION
124 IF(JPARM.EQ. 4) GO TO 140

```

SAM 147
 SAM 148
 SAM 149
 SAM 150
 SAM 151
 SAM 152
 SAM 153
 SAM 154
 SAM 155
 SAM 156
 SAM 157
 SAM 158
 SAM 159
 SAM 160
 SAM 161
 SAM 162
 SAM 163
 SAM 164
 SAM 165
 SAM 166
 SAM 167
 SAM 168
 SAM 169
 SAM 170
 SAM 171
 SAM 172
 SAM 173
 SAM 174
 SAM 175
 SAM 176
 SAM 177
 SAM 178
 SAM 179
 SAM 180
 SAM 181
 SAM 182
 SAM 183
 SAM 184
 SAM 185
 SAM 186
 SAM 187
 SAM 188
 SAM 189
 SAM 190
 SAM 191
 SAM 192
 SAM 193
 SAM 194
 SAM 195
 SAM 196
 SAM 197
 SAM 198
 SAM 199


```

420 JS=IPARM+1
    DO 129 J=JS,3
129 IPARM(J)=0
130 J1=0
    J2=1
    J3=1
    JV=0
    GO TO 136
135 IF(IPARM.EQ.0) GO TO 369
136 JV=JV+1
C*****WRITE TITLE FOR RUN IF NEEDED
    IF(JCIT.GT.0) WRITE(UNIT,202) JV,TITLE
202 FORMAT(2H 1,12,18A6)
C*****INCREMENT PARAMETER INDICES
    J1=J1+1
    IF(J1.LE. IPARM(1)) GO TO 140
    J1=1
    J2=J2+1
    IF(J2.LE. IPARM(2)) GO TO 140
    J2=1
    J3=J3+1
    IF(J3.GT. IPARM(3)) GO TO 369
140 CONTINUE
C*****INITIALIZE MAIN DRIVE
    IGO=0
    ILOT=0.0
    ISTOP=0
    IMIN=0
C*****INITIALIZE FLAGS
    DO 142 J=1,6
    IMU(J)=.FALSE.
142 AFLAG(J)=1
    DO 143 J=1,20
143 PFLAG(J)=0
    ILOTL=0
C*****BRANCH TO INITIALIZE A/C
    IF(JAC.EQ.2) GO TO 147
C*****INITIALIZE A/C + MAIN DRIVE
    THROT=THROTS
    TIME=0.
    IJ=1
    IJX=0
C*****LOAD STATES
    DO 145 J=1,12
145 RAC(J)=SVST(J)
    GO TO 147
C*****LOAD PARAMETERS IF NECESSARY
147 IF ( I KPEFM.EQ.0) GO TO 152
    WRITE(6,630)
630 FORMAT(19H1LIST OF PARAMETERS)
    DO 150 J=1,IPARM
    WRITE(6,632) (PARM(K),K=1,3),VFARM(J,JX(J))
632 FORMAT(10H1,3A6,3X,1PE15.6)

```

SAM 200
 SAM 201
 SAM 202
 SAM 203
 SAM 204
 SAM 205
 SAM 206
 SAM 207
 SAM 208
 SAM 209
 SAM 210
 SAM 211
 SAM 212
 SAM 213
 SAM 214
 SAM 215
 SAM 216
 SAM 217
 SAM 218
 SAM 219
 SAM 220
 SAM 221
 SAM 222
 SAM 223
 SAM 224
 SAM 225
 SAM 226
 SAM 227
 SAM 228
 SAM 229
 SAM 230
 SAM 231
 SAM 232
 SAM 233
 SAM 234
 SAM 235
 SAM 236
 SAM 237
 SAM 238
 SAM 239
 SAM 240
 SAM 241
 SAM 242
 SAM 243
 SAM 244
 SAM 245
 SAM 246
 SAM 247
 SAM 248
 SAM 249
 SAM 250
 SAM 251
 SAM 252

```

275 IF(JPARM(J).LT.0) GO TO 148
    EXR(JPARM(J))=VPARM(J,JX(J))
    GO TO 150
280 148 IF(IAC.EQ.2) GO TO 149
    GX=1.
    IF(MOD(-JPARM(J)+1,6).GE.4) GX=RAD
    EXR(JPARM(J))=VPARM(J,JX(J))*GX
    GO TO 150
285 149 EXR(JPARM(J))=VPARM(J,JX(J))
    150 CONTINUE
    DO 40 I=1,12
    40 SWZ(I)=FA(I)
    GO 45 I=1,NPARM
    IF(JPARM(I).LT.0) GO TO 5
    45 CONTINUE
    152 CONTINUE
    C*****BRANCH AROUND A/C INIT IF TABLES ARE USED
    IF(IAC.EQ.2) GO TO 153
    C*****INITIALIZE A/C AERODYNAMICS
    CALL INAERO
    C*****INITIALIZE A/C STABILITY COORDINATES
    CALL ADIVA
    C*****INITIALIZE TRAJECTORY STORING POINTER, TIME, AND TITLE IF NEEDED
    IF(ISTOR.EQ.0) GO TO 155
    FUND(1)=TITLE(1)
    FUND(2)=TITLE(2)
    NPIS=0
    TSTOR=TIME
    C*****BLANK OUT PRINT WORDS
    153 DO 154 KK=1,4
    154 ZWORD(KK)=PLANK
    C*****INITIALIZE TRAJECTORY INTERPOLATION IF NEEDED
    IF(IAC.EQ.2) CALL INITN
    CALL OUTPUT
    GO TO 310
    C*****MATH DRIVE ITERATION
    300 CALL SANDOC
    C*****BRANCH TO CALL POLICY FOR A/C TRAJ. TO BE GENERATED
    C*****OR INTERPOLATION IF NOT
    IF(IAC.EQ.2) GO TO 304
    CALL POLICY
    GO TO 303
    304 CALL INITAS
    305 CONTINUE
    IF (KMIN.GT.0) CALL MISSILE(KDUM)
    TIME=TIME+HM
    C*****STORE A/C TRAJECTORY IF NEEDED
    310 IF(ISTOP.EQ.0)OR.TIME.LT.TSTOR GO TO 315
    C*****UPDATE POINTER AND TIME TO STORE
    NPIS=NPIS+1
    TSTOR=TSTOR+.25
    GO 311 J=1,3
    311 X(I,NPIS)=EXR(I)

```

```

425      GO 312 J = 1, 4
      312 MC(J,NPTS)=UNIT(J)
      C*****TURN OFF STORAGE IF NO MORE ROOM
      IF(NPTS.EQ. 44) ISTOP=0
      C*****WRITE DATA SET FOR PLOT IF DESIRED
      315 IF(IPLT.EQ. C.OF. TIME .LT. TPLT) GO TO 322
      IPLT=IPLT+DELOT
      TPLT=TPLT+1
      GO 320 J=1,4
      IF(FLAG(J).LE. 0 ) GO TO 318
      TRU(J)=TRUE
      GO TO 320
      318 RM(J,J)=-1.
      320 CONTINUE
      501 WRITE (10,501) (RA(J,J=1,3), (RM(J,K),J=1,3),K=1,4)
      502 FORMAT(10F10.3)
      C*****END OF ENCOUNTER
      330 WRITE(6,640) TJ
      640 FORMAT(11,16HEND OF ENCOUNTER)
      IF=0
      CALL OUTPUT
      GO TO 300
      C*****END OF ENCOUNTER
      330 WRITE(6,640) TJ
      640 FORMAT(11,16HEND OF ENCOUNTER)
      IF=0
      CALL OUTPUT
      C*****WRITE OUT A/C TRAJECTORY IF NEED BE
      IF(IALCUT.GT. 0) WRITE(14,OUT,700) RUNID,NPTS,
      (CX(IK,IL),IK=1,3), (CY(IK,IL),IK=1,3), IL=1,NPTS)
      1
      C*****WRITE CONTROL DATA SET FOR PLOT IF NECESSARY
      IF(IPLT.EQ. 0 ) GO TO 135
      NVEH=1
      GO 351 J=1,4
      IF(IMC(J)) NVEH=NVEH+1
      351 CONTINUE
      705 WRITE(9,705) TITLE, IFLTL,NVEH,DELOT
      705 FORMAT(18A4/13,11,5H1234,6.2)
      GO TO 135
      C*****END OF TASK
      360 WRITE(6,641)
      641 FORMAT(15H0TASK COMPLETED)
      GO TO 100
      1000 STOP
      END

```


2

PAGE

77/08/04. 14.10.44

FIN 4.64420

 $\text{OP}^3\text{Y} = \mathbf{I}$

SHORT-FOOT THE MISSIL

11

```

500 SER=SQRT(RHO)*PA(4)
    001(1)=(VA(3)*RHO-RA(3)*(FA(1)*VA(1)+FA(2)*VA(2)))/
      1 USRR*FA(4)
    001(2)=(RA(1)*VA(2)-FA(2)*VA(1))/SER
    001(3)=PA(6)
    001(4)=PA(5)
    IF(KFILL.EQ. 0) GO TO 2
    DO 1 J = 1,2
    DO 1 I = 1,4
      1 CC2(I,J)=001(1)
    KFILL=0
    GO TO 4
  2 DO 3 J = 1,2
    DO 3 I = 1,4
      LU(1,I)=(GO2(I,J)-001(1))*TI+001(1)
  3 GO2(I,J)=001(1)
  4 IF(TPCOE.EQ. 2) GO TO 5
    OOS=(OOS-RAGN)*TI2+PA(4)
    LGS=(OOS-OOS3)/HM
    OCS=COS
  5 DO 1000 I=1,20
    IF(MFLAG(I).LE. 0) GO TO 1000
    TM=(TIME-TLCI)
    IF(TM.LT. TF(MFLAG(I))) GO TO 6
    MFLAG(I)=MFLAG(I)+1
    IF(MFLAG(I).LT. 5) GO TO 6
    WRITE(6,2000) I,MN(I),TIME
  2000 FORMAT(11,15H***MISSILE NO.,13,25H SELF DESTRUCTS AT TIME =,F4.3)
    IF(CETIT.GT. 0) WRITE(EDIT,5000) JV,(TITLE(J),J=1,2),I,MN(I),
      1 TIME,(RM(J),J=1,3),(PA(J),J=1,3)
  5000 FORMAT(2H 2,12,2A4,2H *,2I2,7A4)
    IJX=IJ
    IJ=0
    CALL OUTPUT
    MFLAG(I)=0
    NMIN=NMIN-1
    GO TO 1000
  6 IF(OTV.LT. 6.) GO TO 23
    IF(GUIDE.EQ. 1) GO TO 806
    IF(RAR(I).LE. EXTR(94)) GO TO RZ2
  806 IF(MFLAG(I).LT. 3) GO TO 7
    SPQ=PA(5)-PM(5,1)
    IF(RAS(SPO).GE. PI) SPQ=SPQ-SIG(P12,SPO)
    IF(RAS(SPO).LE. .06/PI.AND. ANSTRA(P)-RM(6,1)).LE.
      1.0471) GO TO 7
    WRITE(6,2001) IJ,MN(I),TIME
  2001 FORMAT(11,15H***MISSILE NO.,13,22H BREAKS LOCK AT TIME =,F8.3)
    IF(CETIT.GT. 0) WRITE(EDIT,5001) JV,(TITLE(J),J=1,2),I,MN(I),
      1 TIME,(RM(J),J=1,3),(PA(J),J=1,3)
  5001 FORMAT(2H 2,12,2A4,4H 3,2I2,7A4)
    IJX=IJ
    IJ=0
    CALL OUTPUT

```

```

110 MELAG(I)=0
    NMIN=NMIN-1
    GO TO 1000
111 7 IF (IP .GT. 14.) GO TO 8
    Z1=1400.
    GO TO 10
112 8 IF (IP .GT. 55.) GO TO 9
    Z1=2461.*TM-10054.
    GO TO 10
113 9 Z1=117301.
    GO 10 12 J = 1,2
    ANZ=RM(7-J,I)
    GO 11 K = 1,2
114 10 Z(J,K,I)=(CF2(J,K,I)-ANZ)*TI1*ANZ
115 11 ANZ=DF2(J,K,I)
116 12 CF2(J)=DF2(J,2,I)
    IF (IMCOF .EC. 2) GO TO 13
    Z2=(PM(1,I)*VM(1,I)+PM(2,I)*VM(2,I)+VM(3,I)*VM(3,I))/RM(4,I)
    Z3=003-FM(4,I)
    Z4=772-007C
    Z5=723*41.-773/196200.1
    Z6=774
    IF 776 .LT. 2295.1 Z76=2295.
    IF 776 .GT. 4320.1 Z76=4320.
    Z7=.5*Z75/Z76
    CC1=Z77*CO1(I)
    CC2=Z77*CO1(2)
    Z8=1310.*16.2*TH
    GO TO 15
117 13 CC1=0.
    CC2=0.
    IF (IP .GE. 14.) GO TO 14
    Z8=4920.*48.2*TH
    GO TO 15
118 14 Z8=12467.
119 15 IF (RA(3) .GT. 3280. ) GO TO 19
    CC5=0.
    CC3=0.
    IF 41POOF .EQ. 2) GO TO 16
    CC1=Z71*(CO1(3)-OE2(1)).*(Z77)
    GO TO 20
120 16 IF (IP .GT. 19.71) GO TO 17
    F5V=75.66
    GO TO 18
121 17 F5V=957.76*EXP(-.2*(19-7.1))
122 18 CC1=Z71*(CO1(3)-OE2(1))+F5V
    GO TO 20
123 19 CC1=Z71*(CO1(3)-OE2(1))+CC1
    CC3=Z8*CO1(1)
    CC5=100.*COS(CO1(3))
124 20 SPQ=0.161-0E2(2)
    CC2=Z71*(5P6+CC2)
    IF (AB(C(SPO) .GT. FI) SPQ=0.2-SIGMA(I2,SPQ)

```

SAMI 150
 SAMI 151
 SAMI 152
 SAMI 985
 SAMI 986
 SAMI 987
 SAMI 988
 SAMI 989
 SAMI 990
 SAMI 991
 SAMI 992
 SAMI 993
 SAMI 994
 SAMI 995
 SAMI 996
 SAMI 997
 SAMI 998
 SAMI 999
 SAMI 1000
 SAMI 1001
 SAMI 1002
 SAMI 2993
 SAMI 1004
 SAMI 1005
 SAMI 1006
 SAMI 1007
 SAMI 1008
 SAMI 1009
 SAMI 1010
 SAMI 1011
 SAMI 1012
 SAMI 1013
 SAMI 1014
 SAMI 1015
 SAMI 1016
 SAMI 1017
 SAMI 1018
 SAMI 1019
 SAMI 1020
 SAMI 1021
 SAMI 1022
 SAMI 1023
 SAMI 1024
 SAMI 1025
 SAMI 1026
 SAMI 1027
 SAMI 1028
 SAMI 1029
 SAMI 1030
 SAMI 1031
 SAMI 1032
 SAMI 1033
 SAMI 1034

PAGE 4

77/09/04, 14.10.44

FIN 4.6+420

SUBROUTINE MISSILE 74,74 OPT=1

```

160      CO=7X*ED1(2)
      DO 21 J = 1,2
      X3=2.* (CCX(J)-CO1(J,1))/HM
      CO1(J,1)=CC6(J,1)-X33*113*X13
      CO1(J,1)=CCX(J)
      IF ABS(CCX(J)).GT. 554. ) CCX(J)=.16667*CCX(J)*SIGN(465.,CCX(J))
21      CONTINUE
      CO7=CO1*CO6(1,1)+CO3*CO5
      CO8=CO2+CO6(2,1)+CO4
      DO 22 J = 1,2
      VVS=VV(J,1)
      CO2(J,1)=CO2(J,1)-COY(J)*114*COY(J)
      VV(J,1)=CO2(J,1)+1.2*(CO2(J,1)-CO3(J,1))/HM
      ARU(J)=(VV(J,1)-VVS)/HM
22      GO TO 23
      622  MR2=FAM(1)**2
      ONES(1)=(RA(2)-RM(2,1))*VA(3)-VM(3,1)-(RA(3)-RM(3,1))*
      (VA(2)-VM(2,1))/RRR2
      1  ONES(2)=(RA(3)-RM(3,1))*VA(1)-VM(1,1)-(RA(1)-RM(1,1))*
      (VA(3)-VM(3,1))/RRR2
      1  ONES(3)=(RA(1)-RM(1,1))*VA(2)-VM(2,1)-(RA(2)-RM(2,1))*
      (VA(1)-VM(1,1))/RRR2
      CP=SOPT(VH(1,1)*2+VM(2,1)*2)
      CX=-VM(3,1)/(VM(4,1)*CR)
      VVS=VV(1,1)
      VV(1,1)=LOPES(1)*VM(2,1)-ONES(2)*VM(1,1)/ZCP*EXTR(53)
      ARU(1)=(VV(1,1)-VVS)/HM
      VVS=VV(2,1)
      VV(2,1)=CX*(ONES(1)*VM(1,1)+ONES(2)*VM(2,1)+VM(4,1)/CR*ONES(3))
      1  EXTR(53)
      ARU(2)=(VV(2,1)-VVS)/HM
23      CALL ATMOS(1)
      PYZ=MFLAG(1)
      GO TO (24,25,25,26), PYZ
24      WM=4760.-281.*TM
      T2=6000.
      GO TO 27
25      WM=2623.-28.4*TM
      T2=6000.
      GO TO 27
26      WM=1376.
      T2=0.
      27  ZMS=WM/G
      IF (MX7.E0, 1) GO TO 46
      IF (MX7.E0, 2) GO TO 48
      711=MAGHM(1)
      Z1=1./Z11**2
      SPZ=-.578*.012*TM
      IF (Z11.GT. 2.) GO TO 28
      CF=-.256*1.093*711
      CX1=-.256*.089*711
      EX2=-.06666+.0545*711

```

SAM 1035
SAM 1036
SAM 1037
SAM 1038
SAM 1039
SAM 1040
SAM 1041
SAM 1042
SAM 1043
SAM 1044
SAM 1045
SAM 1046
SAM 1047
SAM 1048
SAM 1049
SAM 1050
SAM 1051
SAM 1052
SAM 1053
SAM 1054
SAM 1055
SAM 1056
SAM 1057
SAM 1058
SAM 1059
SAM 1060
SAM 1061
SAM 1062
SAM 1063
SAM 1064
SAM 1065
SAM 1066
SAM 1067
SAM 1068
SAM 1069
SAM 1070
SAM 1071
SAM 1072
SAM 1073
SAM 1074
SAM 1075
SAM 1076
SAM 1077
SAM 1078
SAM 1079
SAM 1080
SAM 1081
SAM 1082
SAM 1083
SAM 1084
SAM 1085
SAM 1086
SAM 1087

```

215  CX3=-.02*.135*Z11
    60 TO 29
22  CF=-1.334+1.577*Z11
    CX1=-.79+1.156*Z11
    CX2=-.00515+.6329*Z11
    CX3=.04+.085*Z11
29  IF(TH.LE. 47.0) GO TO 31
    SP2=0.0
    IF (Z11.GT. 2.75) GO TO 30
    CF=CF-.0475+.15*Z11
    60 TO 31
30  CF=CF+.207+.057*Z11
31  CF=CF*Z11+.75E-06*(SSA+RH13.10)
    IF(Z11.GT. 1.6) GO TO 32
    CY1=.601-.468*Z11
    60 TO 35
32  IF(Z11.GT. 2.25) GO TO 33
    CY1=.316-.291*Z11
    60 TO 35
33  IF(Z11.GT. 2.75) GO TO 34
    CY1=-.34
    60 TO 35
34  CY1=-6.92+.128*Z11
35  IF(Z11.GT. 3.12) GO TO 36
    CV2=-.0143-.0586*Z11
    60 TO 37
36  CV2=-.2A05-.028*Z11
37  CV3=-5.*CX3
    SP3=0AM(1)/(1140.-3.6*TM)
    IF (FLAG(1).GT.3) SP3=0AM(1)/376.
    IF(0AM(1).LE. 3444.) GO TO 38
    IF(0AM(1).GE. 9040.) GO TO 39
    SP1=10.55556-.0016582*0AM(1)
    60 TO 40
38  SP1=6.911
    60 TO 40
39  SP1=1.
40  SLOPE=(SP1-SP15(1))/HM
    IF(TH.LT. 7.65) SLOPE=-.625E-03
    SP15(1)=SP1
    PU 45 JDUM1 = 1, 8
    SP4=SP1+SLOPE*GM*FLOAT(JCUM1-1)
    NO 42 J = 1,2
    ANZ=ANY(J,1)
    AR00=-VV(J,1)+FLOAT(8 - JDUM1)*AR0(J)*G4
    NO 41 K = 1,2
    LV1(J,K,1)=LV1(K)*LV1(J,K,1)+TX1(K)*LV1(J,K,1)-(AR00-
    1)*LV1(J,K,1)+TX1(K)*AR00-LV1(J,K,1)
    LV1(J,K,1)=AR00
    AR00=LV1(J,K,1)
    LV2(J,K,1)=LV2(K)*LV2(J,K,1)+TX2(K)*LV2(J,K,1)-(ANZ-LV2(J,K,1)
    1)*LV2(K,1)+ANZ-LV2(J,K,1)
    LV2(J,K,1)=ANZ

```



```

41 ANZ=LY2(J,K,I)
   DEL(J,I)=SP4*(C.00517 *LX1(J,2,I)-.016 *LX2(J,2,I)+FLOAT(3-2*J)
   1*OMEG(J,I)*.4,16)
42 IF(IABS(DEL(J,I)).GT. 10.) DEL(J,I)=SIGN(10.,DEL(J,I))
   CNY(I)= (AB(1,I)*CX1+CX2*ABS(AB(2,I))+CX3*DEL(1,I))*Z1
   CNY(2)= (-AB(2,I)*CX1+CX2*ABS(AB(1,I))+CX3*DEL(2,I))*Z1
   CNY(3)= (AB(1,I)*CY1+CY2*ABS(AB(2,I))+CY3*DEL(1,I))*Z1*SP2*CHY(1)
   CNY(4)= (-AB(2,I)*CY1+CY2*ABS(AB(1,I))+CY3*DEL(2,I))*Z1*SP2*
   1CNY(2)
   ANY(1,I)=-GAM(I)*CNY(I)/ZMS
   ANY(2,I)=GAM(I)*CNY(2)/ZMS
   AM1(I)= (17-GAM(I)*C1)/ZMS-G*SX19(I)-C*G(2,I)*V11(3,I)*OMEG(3,I)*
   1V11(2,I)
   AM1(2)=ANY(2,I)-OMEG(3,I)*V11(1,I)+OMEG(1,I)*V11(3,I)
   AM1(3)=G*CX19(I)+ANY(1,I)-OMEG(1,I)*V11(2,I)+OMEG(2,I)*V11(1,I)
   OD(1)=SP3*CNH(1)+.9825*OMEG(2,I)*OMEG(1,I)
   OD(2)=SP3*CNH(2)+.9825*OMEG(3,I)*OMEG(1,I)
   00 43 J = 1,2
   OMEG(J,I)=OMEG(J,I)+.5*GM*(OD(I)+ODS(J,I))
43 ODS(J,I)=OD(J)
   SPQ=OMEG(3,I)/GX19(I)
   OMEG(1,I)=-SPQ*SX19(I)
   X18(I)=X18(I)+GM*SPQ
   X19(I)=X19(I)+GM*OMEG(2,I)
   CX19(I)=COS(X19(I))
   SX19(I)=SIN(X19(I))
   00 44 J = 1,3
   V11(J,I)=V11(J,I)+.5*GM*(AM1(J)+AMIS(J,I))
44 AMIS(J,I)=AM1(J)
   AM(1,I)=ATAN(V11(3,I)/V11(1,I))*DEG
45 AF(2,I)=ATAN(V11(2,I)/V11(1,I))*DEG
   IF (ABS(1,I)-.2*ABS(2,I)).LT. 900.) GO TO 9850
   WRITE(6,6005) TJ,MN(I),TIME
6005 FORMAT(I1,15M,*,*,MISSILE NO.,I3,*,GM GOES UNSTABLE AT TIME =,F4.3)
   1 IF(TIMEIT .GT. 0) WRITE(LEU1,5004) JV,ATIME(I),J=1,2),I,MN(I),
   TIME,(X(I),I,J=1,3),(FA(I),J=1,3)
5004 FORMAT(2H 2,12,204,2H 5,212,7A4)
   TJ=1J
   IJ=0
   CALL OUTPUT
   FLAG(I)=0
   NITE=MIN-1
   GO TO 1000
9800 CONTINUE
   SZ=514*(X18(I))
   CZ=COS(X18(I))
   VM(1,I)=CZ*(CX19(I)*V11(1,I)+SX19(I)*V11(3,I))-SZ*V11(2,I)
   VM(2,I)=-SZ*(CX19(I)*V11(1,I)+SX19(I)*V11(3,I))-CZ*V11(2,I)
   VM(3,I)=SX19(I)*V11(1,I)-CX19(I)*V11(3,I)
   60 TO 51
46 IF(MACH(I).GT. .75 ) GO TO 47
   CF=.24/HACH(I)
   60 TO 53

```

1141 SAM
 1142 SAM
 1143 SAM
 1144 SAM
 1145 SAM
 1146 SAM
 1147 SAM
 1148 SAM
 1149 SAM
 1150 SAM
 1151 SAM
 1152 SAM
 1153 SAM
 1154 SAM
 1155 SAM
 1156 SAM
 1157 SAM
 1158 SAM
 1159 SAM
 1160 SAM
 1161 SAM
 1162 SAM
 1163 SAM
 1164 SAM
 1165 SAM
 1166 SAM
 1167 SAM
 1168 SAM
 1169 SAM
 1170 SAM
 1171 SAM
 1172 SAM
 1173 SAM
 1174 SAM
 1175 SAM
 1176 SAM
 1177 SAM
 1178 SAM
 1179 SAM
 1180 SAM
 1181 SAM
 1182 SAM
 1183 SAM
 1184 SAM
 1185 SAM
 1186 SAM
 1187 SAM
 1188 SAM
 1189 SAM
 1190 SAM
 1191 SAM


```

375      TAY(1)=TMI(2)*TIA(7)+TMI(5)*TIA(8)+TMI(9)*TIA(9)
      TAY(2)=TMI(3)*TIA(1)+TMI(6)*TIA(2)+TMI(9)*TIA(3)
      TAY(3)=TMI(4)*TIA(4)+TMI(6)*TIA(5)+TMI(9)*TIA(6)
      TAY(9)=TMI(3)*TIA(7)+TMI(6)*TIA(8)+TMI(9)*TIA(9)
      CALL CONFUZE
      54 GO TO 100 KWT=1,NHIS
      100 SLOW(KWT)=GDF*2.0*QA/CAPEA*VA(4)**2*WATE(KWT)**(1.0/3.0)
      IF(DFLT-LE,1.0) GO TO 65
      CALL STAB(X0,Y0,Z0,XS,YS,ZS,NONHK,T1)
      IF(T1-LE,1.0) GO TO 57
      IF(RA*Q11).GT.0.0) GO TO 999
      IF(PA*11).LT.RMISS) GO TO 999
      55 DO 56 K=1,NCOMPS
      56 DO 56 LEV=1,NLEVS
      PS(LEV,K)=1.0
      RAUFUZE=.FALSE.
      GO TO 83
      57 THCF=T1+DTCF/HM
      CALL STAB(X0(1,2),Y0(1,2),Z0(1,2),XS(1,2),YS(1,2),ZS(1,2),NONHK,12)
      IF(T2-LE,1.0) GO TO 60
      58 IF(PDCF-GE,1.0) GO TO 55
      CALL SPRAY(TBCF,PSCF)
      DO 59 K=1,NCOMPS
      59 DO 59 LEV=1,NLEVS
      PS(LEV,K)=PDCF*(1.0-PDCF)*PSCF(LEV,K)
      RAUFUZE=.FALSE.
      GO TO 83
      60 IF(T2-GE,TBCF) GO TO 63
      61 DO 62 K=1,NCOMPS
      62 DO 62 LEV=1,NLEVS
      PS(LEV,K)=0.0
      RAUFUZE=.FALSE.
      GO TO 83
      63 IF(PDCF-GE,1.0) GO TO 61
      CALL SPRAY(TBCF,PSCF)
      DO 64 K=1,NCOMPS
      64 DO 64 LEV=1,NLEVS
      PS(LEV,K)=(1.0-PDCF)*PSCF(LEV,K)
      RAUFUZE=.FALSE.
      GO TO 83
      65 TBRF=DELTA+DTBRF/HM
      CALL STAB(X0,Y0,Z0,XS,YS,ZS,NONHK,T1)
      IF(T1-LE,1.0) GO TO 68
      CALL SPRAY(TBRF,PSRF)
      66 DO 67 K=1,NCOMPS
      67 DO 67 LEV=1,NLEVS
      PS(LEV,K)=TBRF*(1.0-TBRF)*PSRF(LEV,K)
      RAUFUZE=.TRUE.
      GO TO 83
      68 THCF=T1+DTCF/HM
      CALL STAB(X0(1,2),Y0(1,2),Z0(1,2),XS(1,2),YS(1,2),ZS(1,2),NONHK,12)
      IF(T2-LE,1.0) GO TO 74
      IF(DFLT-GE,11) GO TO 74

```

SAMI 188
 SAMI 189
 SAMI 190
 SAMI 191
 SAMI 192
 SAMI 193
 SAMI 194
 SAMI 195
 SAMI 196
 SAMI 197
 SAMI 198
 SAMI 199
 SAMI 200
 SAMI 201
 SAMI 202
 SAMI 203
 SAMI 204
 SAMI 205
 SAMI 206
 SAMI 207
 SAMI 208
 SAMI 209
 SAMI 210
 SAMI 211
 SAMI 212
 SAMI 213
 SAMI 214
 SAMI 215
 SAMI 216
 SAMI 217
 SAMI 218
 SAMI 219
 SAMI 220
 SAMI 221
 SAMI 222
 SAMI 223
 SAMI 224
 SAMI 225
 SAMI 226
 SAMI 227
 SAMI 228
 SAMI 229
 SAMI 230
 SAMI 231
 SAMI 232
 SAMI 233
 SAMI 234
 SAMI 235
 SAMI 236
 SAMI 237
 SAMI 238
 SAMI 239
 SAMI 240

PAGE 9

77/00/04. 14.10.46

FTN 4.6+420

EXPLODING MISSILE 74/74 OPT=1

```

425 CALL SPRAY(TIME,PSRF)
    IF (POCF.GE.1.0) GO TO 66
    IF (TRF.EQ.1) GO TO 72
    CALL SPRAY(TIME,PSCF)
    IF (TRF.GT.1) GO TO 70
    DO 69 K=1,NCOMPS
    GO 69 LEV=1,NLEVS
430 69 PS(LEV,K)=POCF*POCF*(1.0-POCF)*PSF(LEV,K)*POCF*(1.0-POCF)*
    PSF(LEV,K)
    RADFUZE=.TRUE.
    GO TO 83
435 70 DO 71 K=1,NCOMPS
    DO 71 LEV=1,NLEVS
    71 PS(LEV,K)=POCF*POCF*(1.0-POCF)*PSF(LEV,K)*POCF*(1.0-POCF)*
    PSF(LEV,K)
    RADFUZE=.TRUE.
    GO TO 83
440 72 DO 73 K=1,NCOMPS
    DO 73 LEV=1,NLEVS
    73 PS(LEV,K)=POCF*POCF*(1.0-POCF)*PSF(LEV,K)
    RADFUZE=.TRUE.
    GO TO 83
445 74 IF (T2.GT.1) GO TO 77
    IF (T2.LE.1) GO TO 61
    CALL SPRAY(TIME,PSRF)
    75 DO 76 K=1,NCOMPS
    DO 76 LEV=1,NLEVS
    76 PS(LEV,K)=POCF*POCF*(1.0-POCF)*PSF(LEV,K)
    RADFUZE=.TRUE.
    GO TO 83
450 77 IF (T2.LE.1) GO TO 63
    IF (T2.GT.1) GO TO 63
    CALL SPRAY(TIME,PSRF)
    IF (POCF.GE.1.0) GO TO 75
    IF (TRF.EQ.1) GO TO 81
    CALL SPRAY(TIME,PSCF)
    IF (TRF.GT.1) GO TO 79
    DO 78 K=1,NCOMPS
    DO 78 LEV=1,NLEVS
455 78 PS(LEV,K)=POCF*POCF*(1.0-POCF)*PSF(LEV,K)*POCF*(1.0-POCF)*PSF(LEV,K)
    RADFUZE=.TRUE.
    GO TO 83
460 79 DO 80 K=1,NCOMPS
    DO 80 LEV=1,NLEVS
    80 PS(LEV,K)=POCF*POCF*(1.0-POCF)*PSF(LEV,K)*POCF*(1.0-POCF)*PSF(LEV,K)
    RADFUZE=.TRUE.
    GO TO 83
465 81 DO 82 K=1,NCOMPS
    DO 82 LEV=1,NLEVS
    82 PS(LEV,K)=POCF*POCF*(1.0-POCF)*PSF(LEV,K)
    RADFUZE=.TRUE.
    83 DO X=HP*(1.0-DEL)
    TIME=TIME+HMD-DEL
    
```

SAMI 241
 SAMI 242
 SAMI 243
 SAMI 244
 SAMI 245
 SAMI 246
 SAMI 247
 SAMI 248
 SAMI 249
 SAMI 250
 SAMI 251
 SAMI 252
 SAMI 253
 SAMI 254
 SAMI 255
 SAMI 256
 SAMI 257
 SAMI 258
 SAMI 259
 SAMI 260
 SAMI 261
 SAMI 262
 SAMI 263
 SAMI 264
 SAMI 265
 SAMI 266
 SAMI 267
 SAMI 268
 SAMI 269
 SAMI 270
 SAMI 271
 SAMI 272
 SAMI 273
 SAMI 274
 SAMI 275
 SAMI 276
 SAMI 277
 SAMI 278
 SAMI 279
 SAMI 280
 SAMI 281
 SAMI 282
 SAMI 283
 SAMI 284
 SAMI 285
 SAMI 286
 SAMI 287
 SAMI 288
 SAMI 289
 SAMI 290
 SAMI 291
 SAMI 292
 SAMI 293


```

535 DO 87 LEV=1,NLEVS
      DO 87 L=1,LEND
        PS(LEV,L)=PS(LEV,L)*PS(LEV,L)-PS(LEV,L)*PS(LEV,L)
        PS(LFVAL,L)=1.0
        CPST(LEV,L)=CPST(LEV,L)*CPST(LEV,L)-CPST(LEV,L)*CPST(LEV,L)
      87 CPST(LEV,L)=1.0
      88 DO 89 LEV=1,NLEVS
        PSAC=1.0
        CPSAC=1.0
        DO 89 K=1,NCOMPS
          PSAC=PSAC*PS(LEV,K)
          CPSAC=CPSAC*CPST(LEV,K)
          CPKAC(LEV)=1.0-CPSAC
        89 CPKAC(LEV)=1.0-CPSAC
        WRITE(6,4005)((HEAD04(J),J=1,3),LEV=1,NLEVS)
        WRITE(6,4006)((KLEW(J),J=1,20),LEV=1,NLEVS)
        WRITE(6,4007)((HEAD05(J),J=1,3),LEV=1,NLEVS)
        WRITE(6,4008)((HEAD06(J),J=1,3),LEV=1,NLEVS)
        WRITE(6,4009)((HEAD07(J),J=1,3),LEV=1,NLEVS)
        WRITE(6,4010)((HEAD08(J),J=1,3),LEV=1,NLEVS)
        WRITE(6,4011)((KPAK(LEV),CPKAC(LEV),LEV=1,NLEVS)
        4007 FORMAT(8X,4F14.3,F17.3))
        WRITE(6,4002)((HEAD04(J),J=1,3),LEV=1,NLEVS)
        LJ=1
        LJX=0
        MFLAG(1)=0.0
        NMN=NMN-1
        IF(LEDT.GT.0) WRITE(4,LEDT,5002)JV,(TITLE(J),J=1,20),I,HN(1),
          5002 FORMAT(' 2",12,2A6," 2",212,14A4)
          999 XCMOLC(1)=XCM
          YCMOLC(1)=YCM
          ZCMOLC(1)=ZCM
        1000 CONTINUE
        RETURN
        ENTRY MISINT
        WRITE(6,3000)
        5000 FORMAT(25H0*****MISSILE TYPE 2*****
          NX5=0
          AFAM=2.01
          TT1=LXP(-HM*10.)
          TT2=EXP(-HM*2.)
          TT3=LXP(-HM/.22)
          TT4=EXP(-HM)
          GM=HM*.125
          TX1(1)=EXP(-GM*10.)
          TX1(2)=TX1(1)
          TX2(1)=EXP(-GM*.16)
          TX2(2)=TX1(1)
          TX3(1)=1.-TX1(1)
          TX3(2)=TX1(1)

```

PAGE 12

77/08/04. 14.10.46

FIN 4.64420

OPT=1

74/74

SUBROUTINE MISSIL

```

C05  RT1(1)=.1/GM
C06  RT1(2)=RT1(1)
C07  TX2(1)=1.-TX2(1)
C08  TX2(2)=TX1(1)
C09  RT2(1)=.18/GM
C10  RT2(2)=RT1(2)
C11  HNS=NP
C12  RETURN
C13  ENTRY LAUNCH
C14  DO 1500 J = 1, 20
C15  IF (MFLAG(J) .NE. 0) GO TO 1501
C16 1500 CONTINUE
C17  KA=0
C18  RETURN
C19  DO 1502 L=1,6
C20 1502 RM(L,K)=0.
C21  VM(L,K)=10.
C22  V11(1,K)=10.
C23  V11(2,K)=0.
C24  V11(3,K)=0.
C25  PACHM(K)=0.0
C26  RHO=RA(1)**2+RA(2)**2
C27  VM(5,K)=RA(5)*7.*(RA(1)*VA(2)+RA(2)*VA(1))/RHO
C28  VM(6,K)=.2E24*.992*(RA(5)+7.*(VA(1)*PHO-RA(3)*(RA(1)*VA(1)+RA(2)*VA
C29  1(2)))/(PHO*PA(4)**2))
C30  IF (CAES(VM(5,K)) .GT. PI) VM(5,K)=VM(5,K)-SIGN(2.*PI,VM(5,K))
C31  CALL COORD(VM(1,K),2)
C32  MFLAG(K)=1
C33  RAH(K)=RA(4)
C34  RAND(K)=0.
C35  NMEN=NTIN*1
C36  NX5=NX5+1
C37  MUCK=NX5
C38  IF (IT .GT. 0) WRITE(EDIT,5003) JV,(TITLE(J),J=1,2),I,MN(3),
C39  TIME,(RA(I),J=1,3)
C40 5003 FORMAT(2H 2,12,204,2H 1,212,4A4)
C41  X18(K)=-VM(5,K)
C42  X19(K)=VM(6,K)
C43  SX19(K)=SIN(X19(K))
C44  CX19(K)=COS(X19(K))
C45  C75(K)=SIN(X18(K))
C46  C75(K)=COS(X18(K))
C47  DO 1503 JI=1,2
C48  DELC(JI,K)=0.0
C49  VV(JI,K)=0.0
C50  ANV(JI,K)=0.
C51  CP1(JI,K)=0.
C52  CP2(JI,K)=0.
C53  COSC(JI,K)=0.
C54  APC(JI,K)=0.0
C55  OPCS(JI,K)=0.0
C56  CC(CJI,K)=0.

```

SAM 1283
SAM 1284
SAM 1285
SAM 1286
SAM 1287
SAM 1288
SAM 1289
SAM 1290
SAM 1291
SAM 1292
SAM 1293
SAM 1294
SAM 1295
SAM 1296
SAM 1297
SAM 1298
SAM 1299
SAM 1300
SAM 1301
SAM 1302
SAM 1303
SAM 1304
SAM 1305
SAM 1306
SAM 1307
SAM 1308
SAM 1309
SAM 1310
SAM 1311
SAM 1312
SAM 1313
SAM 1314
SAM 1315
SAM 1316
SAM 1317
SAM 1318
SAM 1319
SAM 1320
SAM 1321
SAM 1322
SAM 1323
SAM 1324
SAM 1325
SAM 1326
SAM 1327
SAM 1328
SAM 1329
SAM 1330
SAM 1331
SAM 1332
SAM 1333
SAM 1334
SAM 1335

```

640      CC2(J1,K)=0.
        DO 1503 J2=1,2
          DP2(J1,J2,K)=VM(7-J1,K)
          LX1(J1,J2,K)=0.0
          LX2(J1,J2,K)=0.0
          LX1(J1,J2,K)=0.
          LX2(J1,J2,K)=0.
1503      TL(K)=TIME
        LO 1504 J = 1.1
        VMS(J,K)=VM(J,K)
        AMIS(J,K)=0.
1504      CHEG(J,K)=0.
        KA=K
        IF(NMIN.GT. 1) RETURN
        CUI=PA14)
        UNIS=LO3
        KFILL=1
        RETURN
        END
650
655

```

```

SAM 1336
SAM 1337
SAM 1338
SAM 1339
SAM 1340
SAM 1341
SAM 1342
SAM 1343
SAM 1344
SAM 1345
SAM 1346
SAM 1347
SAM 1348
SAM 1349
SAM 1350
SAM 1351
SAM 1352
SAM 1353
SAM 1354

```



```

1  SUPROUTINE SPRAY(ULT,PSO)
   COMMON /DRIVE/ TIME,MM,ISTART,TOTAL,EXTR(60),IEXTR(30),ITITLE(18),
   10FC,6,PI,PAO
   COMMON /MISSL/ RM(6,20),VH(6,20),MACHM(20),OAM(20),SSA,AREAM,
5  1VW(2,20),DEL(2,20),AB(2,20),MN(20),RAP(20),RAPD(20)
   COMMON /FLAGS/ JFOL,KFOL,JSAM,KSAH,LSAN,MNIN,ISTOP,IAC,IEDIT,
   1IGUIDF,IMODE,MFLAG(20),JV
   COMMON /AIRCF/ RA(6),VA(6),DUM(16),TIA(9)
   COMMON /CONF/ NCOMPS,NLEVS,NMWS,NSHLOS,NBLAST,NGLIT,THA,PCHA,VE,
10  1DELT,XCH,YCM,ZCM,VNEHI,I
   COMMON /TMO/ XGL(25),YGL(25),ZGL(25),XSH(25),YSH(25),ZSH(25),
   1ASH(25),BSH(25),CSH(25),XUL(25),YUL(25),ZUL(25),ABL(25),EBL(25),
   2COL(25),XCHOLD(20),YCHOLD(20),ZCHOLD(20),FX(25),FY(25),ZEE(25),
   3TAM(9),TMI(9)
   COMMON /FIVE/ VUL(2,11,72),STEAR(19),FRACT(10),SLOW(10)
15  DIMENSION PSO(4,25),SUM(4),VT(3),VS(3)
   DELTA=0.5/VA(4)
   XSTAR=XCHOLD(1)+DLT*(XCM-XCHOLD(1))
   YSTAR=YCHOLD(1)+DLT*(YCM-YCHOLD(1))
   ZSTAR=ZCHOLD(1)+DLT*(ZCM-ZCHOLD(1))
   IF(NBLAST,LT,1) GO TO 102
   GO TO 101 M=1,NBLAST
   IF((XSTAR-XBL(M))/DEL(M))**2+((YSTAR-YBL(M))/DEL(M))**2+
25  1((ZSTAR-ZBL(M))/DEL(M))**2.GT.1.0) GO TO 101
   DO 100 K=1,NCOMPS
   DO 100 LEV=1,NLEVS
190  PSO(LEV,K)=0.0
   RETURN
101 CONTINUE
30  VT(1)=TIA(1)*VA(1)+TIA(2)*VA(2)+TIA(3)*VA(3)
   VT(2)=TIA(4)*VA(1)+TIA(5)*VA(2)+TIA(6)*VA(3)
   VT(3)=TIA(7)*VA(1)+TIA(8)*VA(2)+TIA(9)*VA(3)
   VS(1)=TIA(1)*VM(1,1)+TIA(2)*VM(2,1)+TIA(3)*VM(3,1)
   VS(2)=TIA(4)*VM(1,1)+TIA(5)*VM(2,1)+TIA(6)*VM(3,1)
   VS(3)=TIA(7)*VM(1,1)+TIA(8)*VM(2,1)+TIA(9)*VM(3,1)
   VVS=VT(1)*VS(1)+VT(2)*VS(2)+VT(3)*VS(3)
   A=VA(4)**2+VM(4,1)**2-VE**2-2.0*VTVS
   VRAT=VE/VM(4,1)
   VRAT2=VRAT**2
   DO 31 K=1,NCOMPS
40  DX=EX(K)-XSTAR
   DY=MY(K)-YSTAR
   DZ=ZE(K)-ZSTAR
   R=Z.0*(DX*(VT(1)-VS(1))+DY*(VT(2)-VS(2))+DZ*(VT(3)-VS(3)))
45  C=DX**2+DY**2+DZ**2
   D=0.0*R-4.0*A*C
   IF(D.GE.0.0) GO TO 3
   DO 2 LEV=1,NLEVS
2  PSO(LEV,K)=1.0
   GO TO 31
3  T1=(-D+SQR(D))/(2.0*A)
   T2=(-D-SQR(D))/(2.0*A)
   IF(T1.GE.0.0) GO TO 4

```

SAM 1941
 SAM 382
 SAM 383
 SAM 1942
 SAM 1943
 SAM 1944
 SAM 1945
 SAM 384
 SAM 1947
 SAM 385
 SAM 1949
 SAM 1950
 SAM 1951
 SAM 1952
 SAM 386
 SAM 1953
 SAM 387
 SAM 1954
 SAM 1955
 SAM 1956
 SAM 388
 SAM 1957
 SAM 1958
 SAM 1959
 SAM 1960
 SAM 1961
 SAM 1962
 SAM 1963
 SAM 1964
 SAM 389
 SAM 1966
 SAM 1967
 SAM 1968
 SAM 1969
 SAM 1970
 SAM 1971
 SAM 1972
 SAM 390
 SAM 391
 SAM 1973
 SAM 1974
 SAM 1975
 SAM 1976
 SAM 1979
 SAM 1980
 SAM 1981
 SAM 1982
 SAM 1983
 SAM 1984
 SAM 1985
 SAM 1986
 SAM 1987
 SAM 1988

```

55 IF(T2,LT,0.0) GO TO 1
   TEST=T2
   GO TO 6
60 IF(T2,GT,0.0) GO TO 5
   TEST=T1
   GO TO 6
   5 TEST=AMIN(T1,T2)
   6 DO 7 LEV=1,NLEVS
   7 SUM(LEV)=0.0
     DO 28 KWT=1,NKWS
       KCUNT=0
       8 FLX=DX*VT(1)*TEST
       ELY=OY*VT(2)*TEST
       FLZ=OZ*VT(3)*TEST
       FL=SQRT(ELX**2+ELY**2+ELZ**2)
       KCUNT=KCUNT+1
       PLTAX=ELX/EL
       PLTAY=ELY/EL
       PLTAZ=ELZ/EL
       ELDOJ=BETAX*VT(1)+BETAY*VT(2)+BETAZ*VT(3)
       CUSGAP=(BETAZ*VS(1)+BETAY*VS(2)+BETAZ*VS(3))/VH(4,1)
       VZERO=VH(4,1)*COSGAP/SQRT((VH(4,1)*COSGAP)**2+VE**2-VH(4,1)**2)
       F=SLOW(KWT)*EL-ALOG(1.0+SLOW(KWT)*VZERO*TEST)
       VDOOT=VZERO*(VTVS-ELDOJ-VH(4,1)*COSGAP)/
         1(1.0+(VZERO-VH(4,1)*COSGAP))
       FPRIME=SLOW(KWT)*ELDOJ-(VZERO*VDOOT*TEST)/
         1(1.0+SLOW(KWT)*VZERO*TEST)
       IF(FPRIME-GE,0.0) GO TO 28
       INFW=TEST-F/FPRIME
       IF(INFW,LT,0.0) GO TO 28
       IF(ABS(TNEW-TEST).LE,DELTA) GO TO 10
       IF(KCUNT,GT,10) GO TO 28
       9 TEST=TNEW
       GO TO 8
       10 SLOW=EXP(-SLOW(KWT)*FL)
       COSTHT=(VZERO*COSGAP-VH(4,1))/VF
       IF(ABS(COSTHT),GT,1.0) COSTHT=SIGN(1.0,COSTHT)
       XIG=VT(1)*TEST
       YIG=VT(2)*TEST
       ZIG=VT(3)*TEST
       IF(NSHLOS,LT,1) GO TO 15
       IF(BETAX,EQ,0.0) GO TO 9
       DO 14 L=1,NSHLOS
         IF(EX(K).NE,XSH(L)) GO TO 11
         IF(MY(K).NE,YSH(L)) GO TO 11
         IF(ZEE(K).EQ,ZSH(L)) GO TO 14
       11 OY=(XSH(L)+XIG-XSTAR)/ASH(L)
         OY=(YSH(L)+YIG-YSTAR)/BSH(L)
         OZ=(ZSH(L)+ZIG-ZSTAR)/CSH(L)
         TAY=(BETAY*ASH(L))/(BETAX*BSH(L))
         TXZ=(BETAZ*ASH(L))/(BETAX*CSH(L))
         A=1.0+TXY**2+TXZ**2
         F=-2.0*(OY+TAY*OY+TXZ*OZ)

```

SAM 1989
 SAM 1990
 SAM 1991
 SAM 1992
 SAM 1993
 SAM 1994
 SAM 1995
 SAM 1996
 SAM 1997
 SAM 1998
 SAM 1999
 SAM 2000
 SAM 2001
 SAM 2002
 SAM 2003
 SAM 2004
 SAM 2005
 SAM 2006
 SAM 2007
 SAM 2008
 SAM 2009
 SAM 2010
 SAM 2011
 SAM 2012
 SAM 2013
 SAM 2014
 SAM 2015
 SAM 2016
 SAM 2017
 SAM 2018
 SAM 2019
 SAM 2020
 SAM 2021
 SAM 2022
 SAM 2023
 SAM 2024
 SAM 2025
 SAM 2026
 SAM 2027
 SAM 2028
 SAM 392
 SAM 2030
 SAM 2031
 SAM 2032
 SAM 2033
 SAM 2034
 SAM 2035
 SAM 2036
 SAM 2037
 SAM 2038
 SAM 2039
 SAM 2040
 SAM 2041

```

110 C=0X**2+0Y**2+0Z**2-1.0
    D=0*8-4.0*0.0
    IF(D.LE.0.01) GO TO 14
    C=SQRT(D)
    DO 13 LL=1,2
      XDIR=(-B+D*(1.0**LL))/(2.0*A)
      XPUNCH=XSTAR+XDIR*ASHUL
      IF(XPUNCH.LE.XSTAR) GO TO 12
      IF(X(K)*XIG-XSTAR.GT.XPUNCH) GO TO 28
      GO TO 13
12 IF(X(K)*XIG-XSTAR.LT.XPUNCH) GO TO 28
13 CONTINUE
14 CONTINUE
15 IHEA=ATAN2(SQRT(1.0-COSTHT**2),COSTHT)
    KANG=14.0*THE TA/PI+1.0
    IF(KANG.NE.19) GO TO 16
    STR=STEAR(19)
    GO TO 17
16 STR=STEAR(KANG)+(STEAR(KANG+1)-STEAR(KANG))*
    1(14.0*THE TA/PI+1.0-KANG)
17 VHT=VZERO*SDOWN
    VNET=SQRT((VHT*DE TAX-VT(1))**2+(VHT*BETAY-VT(2))**2)
    1(VHT*DE TAX-VT(3))**2)
    KV=10.9*VNET/VNETHI+1.0
    SPREAD=VRAT?AB5(VRAT*COSTHT)/(VRAT*2.0*VRAT*COSTHT+1.0)**1.5
    DO 27 IXYZ=1,3
      IF(IXYZ-2)18,20,22
18 SHAD=AB5(BETAY)
      IF(BETAX.GE.0.0) GO TO 19
      IFACE=1
      GO TO 24
19 IFACE=0
      GO TO 24
20 SHAD=AB5(BETAY)
      IF(BETAY.GE.0.0) GO TO 21
      IFACE=3
      GO TO 24
21 IFACE=2
      GO TO 24
22 SHAD=AB5(BETAY)
      IF(BETAX.GE.0.0) GO TO 23
      IFACE=4
      GO TO 24
23 IFACE=5
      GO TO 24
24 KFAE=6*K-IFACE
      JINDEX=NMTS*(KFAE-1)+KWT
      DO 26 LEV=1,NLEVS
        IF(KV.LI.11) GO TO 25
        VAREA=VUL(LEV,11,JINDEX)
        GO TO 26
25 VAREA=VUL(LEV,KV,JINDEX)+(10.0*VNET/VNETHI+1.0-KV)*
        1(VUL(LEV,KV+1,JINDEX)-VUL(LEV,KV,JINDEX))
26 SUM(LEV)=SUM(LEV)+STR*FRAC(KWT)*VAREA*SHAD/(SPRFAD*EL**2)

```

SAM 2042
 SAM 2043
 SAM 2044
 SAM 2045
 SAM 2046
 SAM 2047
 SAM 2048
 SAM 2049
 SAM 2050
 SAM 2051
 SAM 2052
 SAM 2053
 SAM 2054
 SAM 2055
 SAM 2056
 SAM 2057
 SAM 2058
 SAM 2059
 SAM 2060
 SAM 2061
 SAM 2062
 SAM 2063
 SAM 2064
 SAM 2065
 SAM 2066
 SAM 2067
 SAM 2068
 SAM 2069
 SAM 2070
 SAM 2071
 SAM 2072
 SAM 2073
 SAM 2074
 SAM 2075
 SAM 2076
 SAM 2077
 SAM 2078
 SAM 2079
 SAM 2080
 SAM 2081
 SAM 2082
 SAM 2083
 SAM 2084
 SAM 2085
 SAM 2086
 SAM 2087
 SAM 2088
 SAM 2089
 SAM 2090
 SAM 2091
 SAM 2092
 SAM 2093
 SAM 2094

SUBROUTINE	STAY	74/74	OPT=1	FTN 4.6+420	77/00/04. 14.10.44	PAGE	9
160	27 CONTINUE				SAM	2095	
	28 CONTINUE				SAM	2096	
	DO 30 LEV=1,NLEVS				SAM	2097	
	IF(SUM(LEV),LT,9.0) GO TO 29				SAM	2098	
	PSC(LEV,K)=0.0				SAM	2099	
155	GO TO 30				SAM	2100	
	29 PSC(LEV,K)=EXP(-SUM(LEV))				SAM	2101	
	30 CONTINUE				SAM	2102	
	31 CONTINUE				SAM	2103	
	RETURN				SAM	2104	
170	END				SAM	2105	

77/08/04. 14.10.44 PAGE 1

FTN 4.6+420

SUBROUTINE STAR 74/74 OPT=1

```

1  SUBROUTINE STAR(X0,X0,Z0,XS,YS,ZS,N,DLT)
   COMMON /MISSL/ KM(6,20),VM(6,20),MACH(20),QAM(20),SSA,AREAM,
   1 VV(2,20),DEL(2,20),AE(2,20),HNC(20),RA(20),FAPD(20)
   COMMON /FLAGS/ JPUL,KPOL,JSAM,KSAM,LSAM,NMIN,ISTOP,IAG,IEDIT,
   1 IGUIDE,IMODE,MFLAG(20),JV
   COMMON /AIFCF/ DUM(20),TIA(9)
   COMMON /ONE/ NCOMP,NLEVS,NMTS,NSHLS,NBLAST,NGLIT,TMA,RCHA,VE,
   1 DELT,XCH,YCH,ZCM,VNETHI,I
   COMMON /TWO/ XGL(25),YGL(25),ZGL(25),XSH(25),YSH(25),ZSH(25),
   1 ASH(25),BSH(25),GSH(25),XBL(25),YBL(25),ZBL(25),ABL(25),BBL(25),
   2 CBL(25),XCMOLD(20),YCMOLD(20),ZCMOLD(20),EX(25),WY(25),ZEE(25),
   3 TAN(9),THI(9)
   DIMENSION X0(25),Y0(25),Z0(25),XS(25),YS(25),ZS(25)
   DLT=2.0
   IF(N.LT.1) RETURN
   DX=XCMOLD(I)-XCH
   DY=YCMOLD(I)-YCH
   CZ=ZCMOLD(I)-ZCH
   DO 4 J=1,N
   IF(DZ.EQ.0.0) GO TO 1
   XY2=(XS(J)*YS(J))**2
   XZ2=(XS(J)*ZS(J))**2
   YZ2=(YS(J)*ZS(J))**2
   TYZ=XCH*ZCMOLD(I)-YCMOLD(I)*ZCH+X0(J)*DZ
   YZ=XCH*ZCMOLD(I)-YCMOLD(I)*ZCH+Y0(J)*DZ
   A=XY2*DZ**2+XZ2*DY**2+YZ2*DX**2
   B=-2.0*(DX*YZ2+YXZ*DY+XZ2*YZ*DZ**2+XY2*Z0(J))
   C=XZ2*Y7**2+YZ2*YX7**2+XV2*OZ**2*(Z0(J)**2-ZS(J)**2)
   C=A*B-4.0*A*C
   IF(D.LT.0.0) GO TO 4
   D=SORT(D)
   Z3=(-B+SIGN(D,DZ))/(2.0*A)
   DELL=(ZCMOLD(I)-Z3)/DZ
   GO TO 3
35  1 IF(DY.EQ.0.0) GO TO 2
   A=(YS(J)*DX)**2+(XS(J)*DY)**2
   TXV=XCH*YCMOLD(I)-XCMOLD(I)*YCH+X0(J)*DY
   XY2=(XS(J)*DY)**2
   B=2.0*(YS(J)*TXV)**2+XV2*(Y0(J)-XY2*Y0(J))
   C=(YS(J)*TXV)**2+XY2*(Y0(J)-XY2*Y0(J))**2+YS(J)**2
   1 ((ZCH-Z0(J))/ZS(J))**2-1.0)
   D=9*B-4.0*A*C
   IF(D.LT.0.0) GO TO 4
   D=SORT(D)
   Y3=(-B+SIGN(D,DY))/(2.0*A)
   DELL=(YCMOLD(I)-Y3)/DY
   GO TO 3
45  2 IF(DX.EQ.0.0) RETURN
   TYZ=1.0-((ZCH-Z0(J))/ZS(J))**2-((YCH-Y0(J))/YS(J))**2
   IF(TYZ.LT.0.0) GO TO 4
   TYZ=ABS(TYZ)
   X3=X0(J)+XS(J)*SIGN(TYZ,DX)
   DELL=(XCMOLD(I)-X3)/DX

```

SAM 2106
 SAM 2107
 SAM 2108
 SAM 2109
 SAM 2110
 SAM 2111
 SAM 2112
 SAM 393
 SAM 2114
 SAM 2115
 SAM 2116
 SAM 2117
 SAM 2118
 SAM 2119
 SAM 2120
 SAM 2121
 SAM 2122
 SAM 2123
 SAM 2124
 SAM 2125
 SAM 2126
 SAM 2127
 SAM 2128
 SAM 2129
 SAM 2130
 SAM 2131
 SAM 2132
 SAM 2133
 SAM 2134
 SAM 2135
 SAM 2136
 SAM 2137
 SAM 2138
 SAM 2139
 SAM 2140
 SAM 2141
 SAM 2142
 SAM 2143
 SAM 2144
 SAM 2145
 SAM 2146
 SAM 2147
 SAM 2148
 SAM 2149
 SAM 2150
 SAM 2151
 SAM 2152
 SAM 2153
 SAM 2154
 SAM 2155
 SAM 2156
 SAM 2157
 SAM 2158

SUBROUTINE STAB

74/74 OPT=1

FTN 4.64420

77/08/66. 14.10.44

PAGE

2

3 IF(UELL.LT.0.0) GO TO 4
4 CONTINUE
RETURN
END

SAM 2159
SAM 2163
SAM 2161
SAM 2162
SAM 2163

SUBROUTINE	CCORRUF	I ₄ /74	OPT=1	FTN 4.6+420	77/08/64.	14.10.44	PAGE 1
------------	---------	--------------------	-------	-------------	-----------	----------	--------

```

1  SUBROUTINE CONFUTE
COMMON /HISL/ RH(6,2), VM(6,20), MACMH(20), OMM(20), SSA, APEAH,
1  IWL(2,20), DEL(2,20), AB(2,20), MN(20), RAN(20), RAPD(20)
COMMON /FLAGS/ JPUL, KPUL, JSAM, KSAH, LSAH, RMIN, ISTOP, IAG, IEDIT,
5  IGUIDE, TMODE, MFLAG(20), JV
COMMON /AIRCF/ DUM(24), TIA(9)
COMMON /ONE/ PCOMPS, NLEVS, NMTS, NSHLOS, NBLAST, HGLIT, THA, RCHA, VE,
1  DELT, XCM, YCM, ZCM, VNE, TH1, I
COMMON /THO/ XGL(25), YGL(25), ZGL(25), XSH(25), YSH(25), ZSH(25),
1  ASH(25), PSR(25), CSR(25), XBL(25), YBL(25), ZBL(25), ABL(25), BBL(25),
10  ZCH(25), XCMOLD(20), YCMOLD(20), ZCMOLD(20), EX(25), MY(25), ZEE(25),
2  TAM(9), TH1(9)
REAL XG(2), YG(2), ZG(2)
DELT=2.6
DO 10 IGL=1, NGLIT
11=XGL(IGL)-XCMOLD(I)
12=YGL(IGL)-YCMOLD(I)
13=ZGL(IGL)-ZCMOLD(I)
20  XG(I)=TAM(I)*T1+TAM(2)*T2+TAM(3)*T3
YG(I)=TAM(I)*T1+TAM(5)*T2+TAM(6)*T3
ZG(I)=TAM(I)*T1+TAM(8)*T2+TAM(9)*T3
11=XGL(IGL)-XCM
12=YGL(IGL)-YCM
13=XGL(IGL)-ZCM
25  XG(2)=TAM(1)*T1+TAM(2)*T2+TAM(3)*T3
YG(2)=TAM(4)*T1+TAM(5)*T2+TAM(6)*T3
ZG(2)=TAM(7)*T1+TAM(8)*T2+TAM(9)*T3
IF (THA.GT.0.0) GO TO 1
XG(1)=-XG(1)
YG(1)=-YG(1)
ZG(1)=-ZG(1)
30  CX=XG(1)-XG(2)
CY=YG(1)-YG(2)
CZ=ZG(1)-ZG(2)
IF (CX.NE.0.0) GO TO 4
IF (YG(1).LT.0.0) GO TO 10
IF (XG(1).GT.RCHA) GO TO 10
IF (CZ.NE.0.0) GO TO 2
IF (CY.EQ.0.0) GO TO 10
Y3=XG(1)*THA**2-ZG(1)**2
IF (Y3.LT.0.0) GO TO 10
Y3=SIGN(SQRT(Y3),Y4)
DELT=YG(1)-Y3/DY
IF (DELT.GT.1.0) GO TO 10
IF (DELT.GE.0.0) GO TO 9
CFLIT=(YG(1)+Y3)/DY
GO TO 7
2  A=UY**2+OZ**2
IF MP=YG(1)*ZG(2)-YG(2)*ZG(1)
B=-2.*TEMP*DY
C=TEMP**2-(XG(1)*THA*UZ)**2
D=B**4-A**4
IF (D.LT.0.0) GO TO 10
U=SQRT(D)

```

```

50      Z3=(-B+SIGN(D,Z1))/(2.0*A)
        DELT=(ZG(1)-73)/DZ
        IF(DELTT.LT.0.0) GO TO 3
        IF(DELTT.GT.1.0) 10,9
3      Z3=(-B-SIGN(D,Z1))/(2.0*A)
        DELT=(ZG(1)-73)/DZ
        GO TO 7
60      A=V**2+DZ**2-(DX*THA)**2
        T1=YG(2)*XG(1)-YG(1)*XG(2)
        T2=ZG(2)*XG(1)-ZG(1)*XG(2)
        R=2.0*(T1*CY+T2*OZ)
        C=T1**2+T2**2
        IF(A.NE.0.0) GO TO 5
        IF(R.GE.0.0) GO TO 10
        X3=-C/B
        IF(X3.GT.FCHA) GO TO 10
        DELT=(XG(1)-X3)/DX
        GO TO 7
70      5 C=B*B-4.0*A*C
        IF(D.LT.0.0) GO TO 10
        L=SQRT(D)
        X3=(-B+SIGN(D,A*DX))/(2.0*A)
        IF(X3.LT.0.0) GO TO 10
        IF(X3.GT.FCHA) GO TO 6
        DELT=(XG(1)-X3)/DX
        IF(DELTT.GE.0.0) GO TO 8
80      6 X3=(-B-SIGN(D,A*DX))/(2.0*A)
        IF(X3.LT.0.0) GO TO 10
        IF(X3.GT.FCHA) GO TO 10
        DELT=(XG(1)-X3)/DX
7      IF(DELTT.LT.0.0) GC TO 10
8      IF(DELTT.GT.1.0) GO TO 10
9      IF(DELTT.LT.DFLT) DELT=DELT
10     CONTINUE
        RETURN
        END

```

```

SAM      2217
SAM      2218
SAM      2219
SAM      2220
SAM      2221
SAM      2222
SAM      2223
SAM      2224
SAM      2225
SAM      2226
SAM      2227
SAM      2228
SAM      2229
SAM      2230
SAM      2231
SAM      2232
SAM      2233
SAM      2234
SAM      2235
SAM      2236
SAM      2237
SAM      2238
SAM      2239
SAM      2240
SAM      2241
SAM      2242
SAM      2243
SAM      2244
SAM      2245
SAM      2246
SAM      2247
SAM      2248
SAM      2249
SAM      2250
SAM      2251
SAM      2252

```


SECTION 5

DEFINITION OF FORTRAN VARIABLES

The following pages of this section list and define those FORTRAN variables which have been added to the DSAMAM program for the endgame. Also shown is the common block in which the variable is found or, if it is not in common, the subroutine which uses it. Finally, there is an indication as to whether the value of the variable is read as input or computed internally.

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block or Subroutine Where Found</u>	<u>Definition</u>
ABL(I)	Input	/TWO/	For the Ith blast ellipsoid, the length of the semi-axis in the X-direction of the aircraft body system (ft)
ASH(I)	Input	/TWO/	For the Ith fragment shield ellipsoid, the length of the semi-axis in the X-direction of the aircraft body system (ft)
BBL(I)	Input	/TWO/	For the Ith blast ellipsoid, the length of the semi-axis in the Y-direction of the aircraft body system (ft)
BETAX	Internal	SPRAY	Direction cosine with respect to the X-axis of the aircraft body system of the line traversed by the fragment
BETAY	Internal	SPRAY	Direction cosine with respect to the Y-axis of the aircraft body system of the line traversed by the fragment
BETAZ	Internal	SPRAY	Direction cosine with respect to the Z-axis of the aircraft body system of the line traversed by the fragment
BSH(I)	Input	/TWO/	For the Ith fragment shield ellipsoid, the length of the semi-axis in the Y-direction of the aircraft body system (ft)
CBL(I)	Input	/TWO/	For the Ith blast ellipsoid, the length of the semi-axis in the Z-direction of the aircraft body system (ft)
CDR	Input	/THREE/	Fragment drag coefficient

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block or Subroutine Where Found</u>	<u>Definition</u>
COSGAM	Internal	SPRAY	Cosine of the angle between the missile velocity and the velocity vector of the fragment in a dynamic explosion
COSTHT	Internal	SPRAY	Cosine of the angle between the missile velocity vector and the velocity vector of the fragment in a static explosion
CPS(I,J)	Internal	/SIX/	Cumulative survival probability for component J at kill level I
CPKAC(I)	Internal	MISSIL	Cumulative overall aircraft kill probability at kill level I
CPST(I,J)	Internal	MISSIL	Cumulative survival probability for component J at kill level I adjusted for doubly vulnerable pairs in order to calculate overall aircraft kill probability
CSH(I)	Input	/TWO/	For the Ith fragment shield ellipsoid, the length of the semi-axis in the Z-direction of the aircraft body system (ft)
DELT	Internal	/ONE/	That fraction of the time increment between two integration points at which radar fuzing occurs
DTCF	Input	/THREE/	Delay time of the contact fuze (sec.)
DTRF	Input	/THREE/	Delay time of the radar fuze (sec.)
EL	Internal	SPRAY	The distance traveled by a fragment before hitting an aircraft component (ft)

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block or Subroutine Where Found</u>	<u>Definition</u>
ELDOT	Internal	SPRAY	Rate of change of EL with respect to time (ft/sec).
EX(I)	Input	/TWO/	X-coordinate in the aircraft body system of the center of gravity of the Ith vulnerable component (ft).
F	Internal	SPRAY	A function of time whose roots represent solutions for the intersection of the fragment and an aircraft component.
FPRIME	Internal	SPRAY	The rate of change of F with respect to time.
FRACT(I)	Input	/FIVE/	Fraction by number of all fragments belonging to fragment mass class I.
HAFANG	Input	/THREE/	Half-angle of the radar fuze (degrees).
HEAD1(I)	Internal	MISSIL	Printout heading. I has a maximum value of 3.
HEAD2(I)	Internal	MISSIL	Printout heading. I has a maximum value of 3.
HEAD3(I)	Internal	MISSIL	Printout heading. I has a maximum value of 3.
HEAD4(I)	Internal	MISSIL	Printout heading. I has a maximum value of 3.
HEAD5(I)	Internal	MISSIL	Printout heading. I has a maximum value of 3.
HEAD6(I)	Internal	MISSIL	Printout heading. I has a maximum value of 3.
I	Internal	/ONE/	Index which points to the particular missile in the air being considered. This variable is also used as a temporary index in other parts of the program which do not relate to the endgame.

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block of Subroutine Where Found</u>	<u>Definition</u>
KLEV(I,J)	Internal	MISSIL	Printout heading which designates kill level J. I has a maximum value of 2.
NBLAST	Input	/ONE/	Number of blast ellipsoids.
NCOMPS	Input	/ONE/	Number of vulnerable components (including doubly vulnerable components).
NDHK	Input	/THREE/	Number of direct-hit-with-kill ellipsoids.
NDHNK	Input	/THREE/	Number of direct-hit-no-kill ellipsoids.
NDUBLY	Input	/THREE/	Number of <u>pairs</u> of doubly vulnerable components.
NGLIT	Input	/ONE/	Number of glitter points.
NLEVS	Input	/ONE/	Number of kill levels.
NSHLDS	Input	/ONE/	Number of shield ellipsoids.
NWTS	Input	/ONE/	Number of fragment mass classes.
PDCF	Input	/THREE/	Probability that the contact fuze is a dud.
PDRF	Input	/THREE/	Probability that the radar fuze is a dud.
PKAC(I)	Internal	MISSIL	Single-shot overall aircraft kill probability at kill level I.
PS(I,J)	Internal	MISSIL	Single-shot survival probability for component J at kill level I.
PSCF(I,J)	Internal	MISSIL	Single-shot survival probability for component J at kill level I due to detonation initiated by contact fuze.

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block of Subroutine Where Found</u>	<u>Definition</u>
PSRF(I,J)	Internal	MISSIL	Single-shot survival probability for component J at kill level I due to detonation initiated by radar fuze.
RADFUZE	Internal	MISSIL	Indicator set to .TRUE. if radar fuze is activated - otherwise .FALSE.
RCHA	Internal	/ONE/	Maximum range of the radar fuze multiplied by the cosine of the radar fuze half-angle (ft).
RMISS	Input	/THREE/	Range outside of which the missile is considered to have missed after having passed the point of closest approach to the target (ft).
SDOWN	Internal	SPRAY	The fraction of its initial velocity to which a fragment slows down after traveling a distance EL.
SLOW(I)	Internal	/FIVE/	Slowdown constant for fragments of mass class I (ft^{-1}).
SPREAD	Internal	SPRAY	Factor which when multiplied by the dynamic fragment density gives the fragment density for a static explosion.
STEAR(I)	Input	/FIVE/	Static fragment density (fragments/steradian). The index I represents 19 points from 0° to 180° off the nose at 10° intervals.
SUM(I)	Internal	SPRAY	Expected number of hits capable of producing kill level I on a component.

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block of Subroutine Where Found</u>	<u>Definition</u>
TAM(I)	Internal	/TWO/	Transformation matrix between the aircraft body coordinate system and the missile body coordinate system. The index I runs from 1 to 9 starting at the upper left of the matrix and proceeding left to right across the three rows of the matrix.
THA	Internal	/ONE/	Tangent of the radar fuze half-angle.
THETA	Internal	SPRAY	Angle between the missile velocity vector and the fragment velocity vector in a static explosion (radians).
TIA(I)	Internal	/AIRCF/	Transformation matrix between the aircraft body coordinate system and the inertial coordinate system. The index I runs from 1 to 9 starting at the upper left of the matrix and proceeding left to right across the three rows of the matrix.
TMI(I)	Internal	/TWO/	Transformation matrix between the missile body coordinate system and the inertial coordinate system. The index I runs from 1 to 9 starting at the upper left of the matrix and proceeding left to right across the three rows of the matrix.
VE	Input	/THREE/	Fragment static emission speed (ft/sec).
VHIT	Internal	SPRAY	The speed of the striking fragment (ft/sec).

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block of Subroutine Where Found</u>	<u>Definition</u>
VNET	Internal	SPRAY	The net striking speed of the fragment (i.e., the magnitude of the relative velocity vector between the fragment and the aircraft) (ft/sec).
VNETHI	Input	/ONE/	Normalizing velocity for vulnerable area inputs. Values are read for each of the 11 net striking velocities corresponding to 0, 0.1, 0.2, ..., 1.0 times VNETHI (ft/sec).
VODOT	Internal	SPRAY	Rate of change of VZERO with respect to time (ft/sec ²).
VS(I)	Internal	SPRAY	Missile velocity vector in the aircraft body system (ft/sec).
VT(I)	Internal	SPRAY	Aircraft velocity vector in the aircraft body system (ft/sec).
VUL(I,J,K)	Input	/FIVE/	Vulnerable area (ft ²). The index I represents kill level. The index J represents 11 levels of net striking speed. The index K combines aspect, fragment mass class, and component.
VX	Internal	MISSIL	X-component in the inertial coordinate system of the relative velocity vector of the aircraft with respect to the missile (ft/sec).

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block of Subroutine Where Found</u>	<u>Definition</u>
VY	Internal	MISSIL	Y-component in the inertial coordinate system of the relative velocity vector of the aircraft with respect to the missile (ft/sec).
VZ	Internal	MISSIL	Z-component in the inertial coordinate system of the relative velocity vector of the aircraft with respect to the missile (ft/sec).
VZERO	Internal	SPRAY	Magnitude of the dynamic velocity vector of the fragment (ft/sec).
WATE(I)	Input	/FOUR/	Average weight of fragments in mass class I (grains).
WY(I)	Input	/TWO/	Y-coordinate in the aircraft body system of the center of gravity of the Ith vulnerable component (ft.).
XBL(I)	Input	/TWO/	X-coordinate in the aircraft body system of the center of the Ith blast ellipsoid (ft.).
XCG	Internal	MISSIL	X-coordinate in the inertial system of the center of gravity of the aircraft relative to the missile (ft.).
XCM	Internal	/ONE/	X-coordinate in the aircraft body system of the missile currently being considered (ft.).
XCMOLD(I)	Internal	/TWO/	X-coordinate in the aircraft body system of missile I at the previous time step (ft.).

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block of Subroutine Where Found</u>	<u>Definition</u>
XG(I)	Internal	CONFUZE	X-coordinate in the missile body system of the glitter point. The index I is 1 for the previous time pulse and 2 for the current time pulse.
XGL(I)	Input	/TWO/	X-coordinate in the aircraft body system of the Ith glitter point (ft.).
XO(I,J)	Input	/FOUR/	X-coordinate in the aircraft body system of the center of the Ith direct-hit ellipsoid of type J (ft.). The type, J, specifies direct-hit-without kill (J=1) or direct-hit-with-kill (j=2).
XS(I,J)	Input	/FOUR/	For the Ith direct-hit ellipsoid of type J, the length of the semi-axis in the X-direction of the aircraft body system (ft.). The type, J, specifies direct-hit-without-kill (J=1) or direct-hit-with-kill (J=2).
XSH(I)	Input	/TWO/	X-coordinate in the aircraft body system of the center of the Ith fragment shield ellipsoid (ft.).
XSTAR	Internal	SPRAY	X-coordinate in the aircraft body system of the explosion point (ft.).
YBL(I)	Input	/TWO/	Y-coordinate in the aircraft body system of the center of the Ith blast ellipsoid (ft.).

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block of Subroutine Where Found</u>	<u>Definition</u>
YCG	Internal	MISSIL	Y-coordinate in the inertial system of the center of gravity of the aircraft relative to the missile (ft.).
YCM	Internal	/ONE/	Y-coordinate in the aircraft body system of the missile currently being considered (ft.).
YCMOLD(I)	Internal	/TWO/	Y-coordinate in the aircraft body system of missile I at the previous time step (ft.).
YG(I)	Internal	CONFUZE	Y-coordinate in the missile body system of the glitter point. The index I is 1 for the previous time pulse and 2 for the current time pulse.
YGL(I)	Input	/TWO/	Y-coordinate in the aircraft body system of the Ith glitter point (ft.).
YO(I,J)	Input	/FOUR/	Y-coordinate in the aircraft body system of the center of the Ith direct-hit ellipsoid of type J (ft.). The type, J, specifies direct-hit-without-kill (J=1) or direct-hit-with-kill (J=2).
YS(I,J)	Input	/FOUR/	For the Ith direct-hit ellipsoid of type J, the length of the semi-axis in the Y-direction of the aircraft body system (ft.). The type, J, specifies direct-hit-without-kill (J=1) or direct-hit-with-kill (J=2).

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block of Subroutine Where Found</u>	<u>Definition</u>
YSH(I)	Input	/TWO/	Y-coordinate in the aircraft body system of the center of the Ith fragment shield ellipsoid (ft.).
YSTAR	Internal	SPRAY	Y-coordinate in the aircraft body system of the explosion point (ft.).
ZBL(I)	Input	/TWO/	Z-coordinate in the aircraft body system of the center of the Ith blast ellipsoid (ft.).
ZCG	Internal	MISSIL	Z-coordinate in the inertial system of the center of gravity of the aircraft relative to the missile (ft.).
ZCM	Internal	/ONE/	Z-coordinate in the aircraft body system of the missile currently being considered (ft.).
ZCMOLD(I)	Internal	/TWO/	Z-coordinate in the aircraft body system of missile I at the previous time step.
ZEE(I)	Input	/TWO/	Z-coordinate in the aircraft body system of the center of gravity of the Ith vulnerable component (ft.).
ZG(I)	Internal	CONFUZE	Z-coordinate in the missile body system of the glitter point. The index I is 1 for the previous time pulse and 2 for the current time pulse.
ZGL(I)	Input	/TWO/	Z-coordinate in the aircraft body system of the Ith glitter point (ft.).

<u>FORTTRAN Variable</u>	<u>Input or Internal</u>	<u>Common Block of Subroutine Where Found</u>	<u>Definition</u>
ZO(I,J)	Input	/FOUR/	Z-coordinate in the aircraft body system of the center of the Ith direct-hit ellipsoid of type J (ft.). The type, J, specifies direct-hit-without-kill (J=1) or direct-hit-with-kill (J=2).
ZS(I,J)	Input	/FOUR/	For the Ith direct-hit ellipsoid of type J, the length of the semi-axis in the Z-direction of the aircraft body system (ft.). The type, J, specifies direct-hit-without-kill (J=1) or direct-hit-with-kill (J=2).
ZSH(I)	Input	/TWO/	Z-coordinate in the aircraft body system of the center of the Ith fragment shield ellipsoid (ft.).
ZSTAR	Internal	SPRAY	Z-coordinate in the aircraft body system of the explosion point (ft.).